

# Multiphysics Simulation of Particle Clouds in Coating: The long Journey from Modelling to validated Industrial Application



Keynote Address, 17<sup>th</sup> International Conference of Multiphysics  
15<sup>th</sup> Dec 2022, G. Boiger, OSLOMET University, Oslo, Norway



Europe  
Switzerland  
Canton of Zurich  
Winterthur

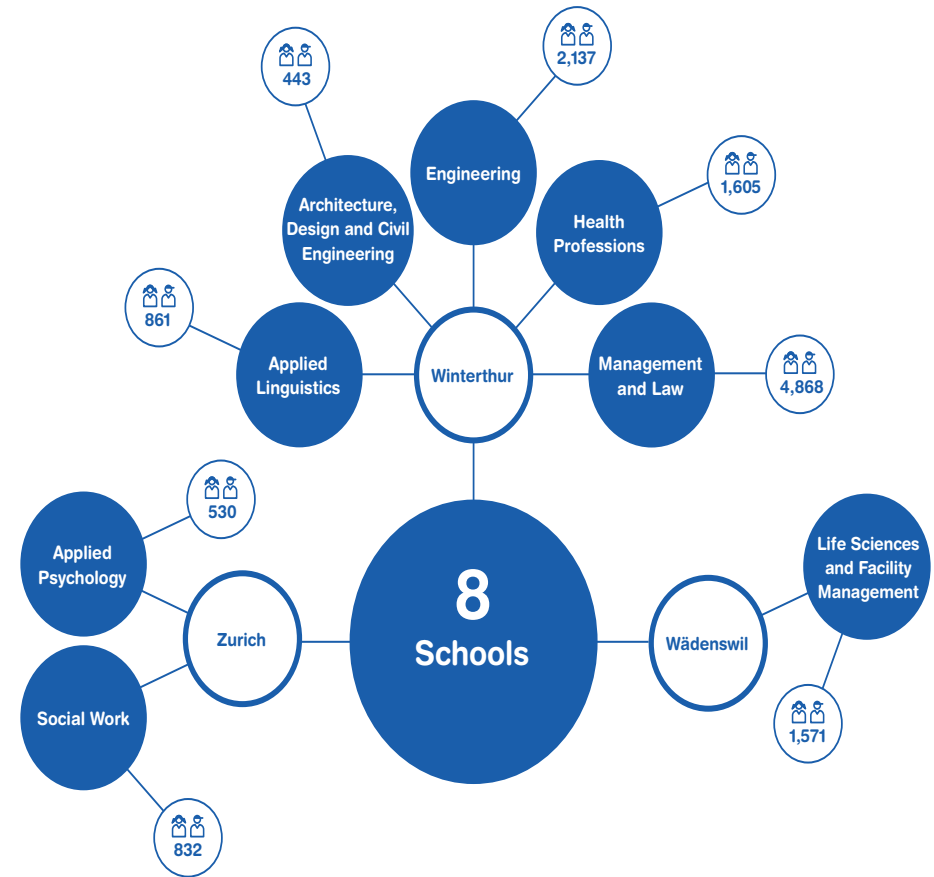


### Gernot Boiger

- Professor of Modelling Multiphysics Applications
- Head of Research Area Multiphysics Modelling and Imaging
- Vice President Europe Int. Soc. Multiphysics
- ZHAW Zurich University of Applied Sciences
- SoE School of Engineering
- ICP Institute of Computational Physics



# Zurich University of Applied Sciences



# Research Area

## Multiphysics Modelling and Imaging

### Multiphysics Modeling



Gernot Boiger, Prof.



Marlon Boldrini, MSc.



Alain Schubiger, MSc.



Viktor Lienhard, MSc.



Vinzenz Muser, MSc.



Multiphysics Modeling  
and Imaging



Bercan Siyahhan, MSc.



Jhimy Rivero



Vincent Buff,  
MSc.  
Zür



Marco Hostettler,  
MSc.



Sima Delbari,  
MSE Student



Darren Sharman,  
MSc.

### Micro Structures & Imaging



Lorenz Holzer, PhD.



Lukas Keller, PhD.



Sebastian Spirig, MSc.



Philip Marmet, MSc.

### FE Thermal- & Fluid- Eng.



Thomas Hocker, Prof.



Yasser Safa, PhD.



Guido Sartoris, PhD.



Sandro Ehrat, MSc.

# Multiphysics Simulation of Particle Clouds in Coating: The long Journey from Modelling to validated Industrial Application



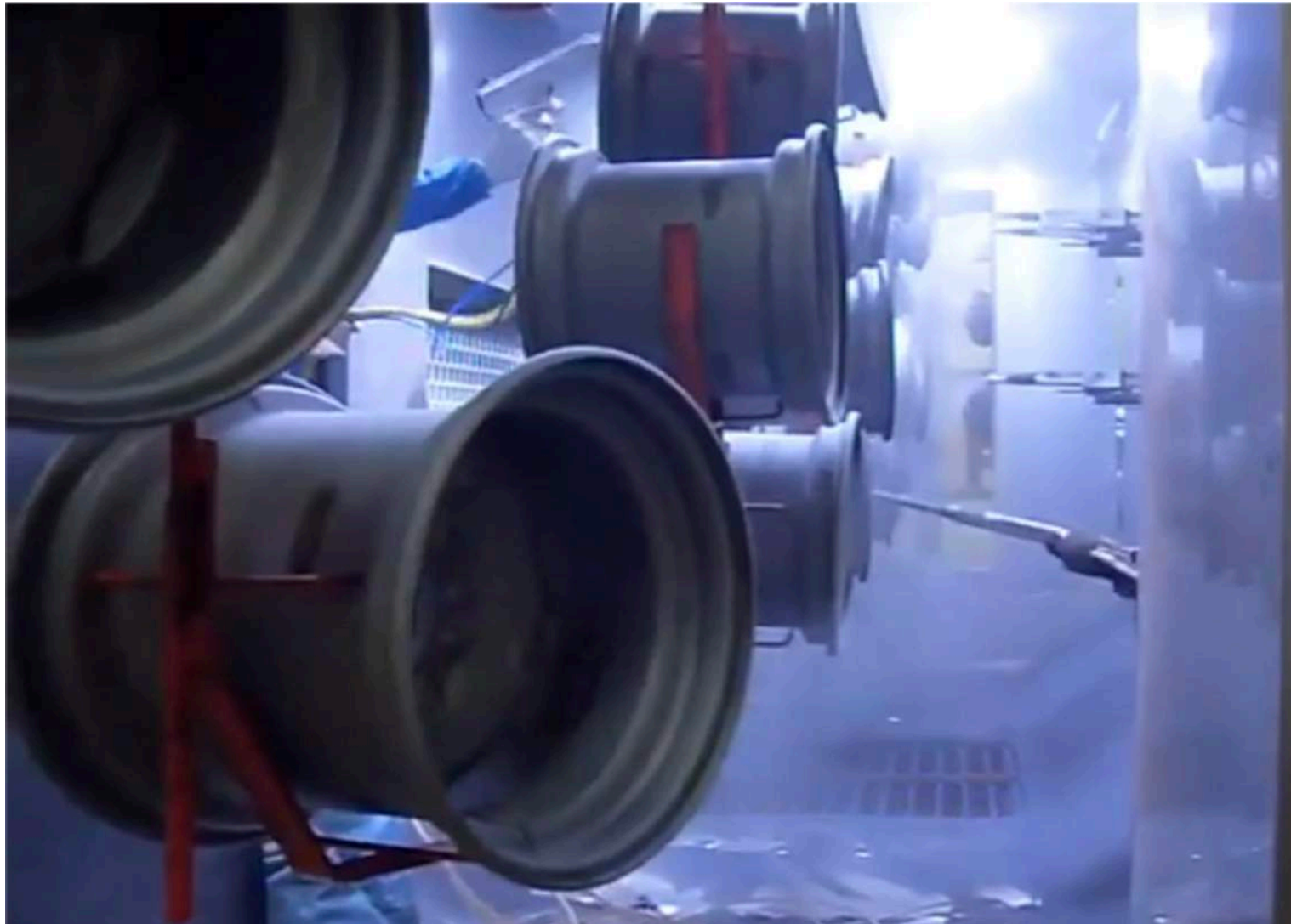
Keynote Address, 17<sup>th</sup> International Conference of Multiphysics  
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# 1. Overview & Introduction

# Content

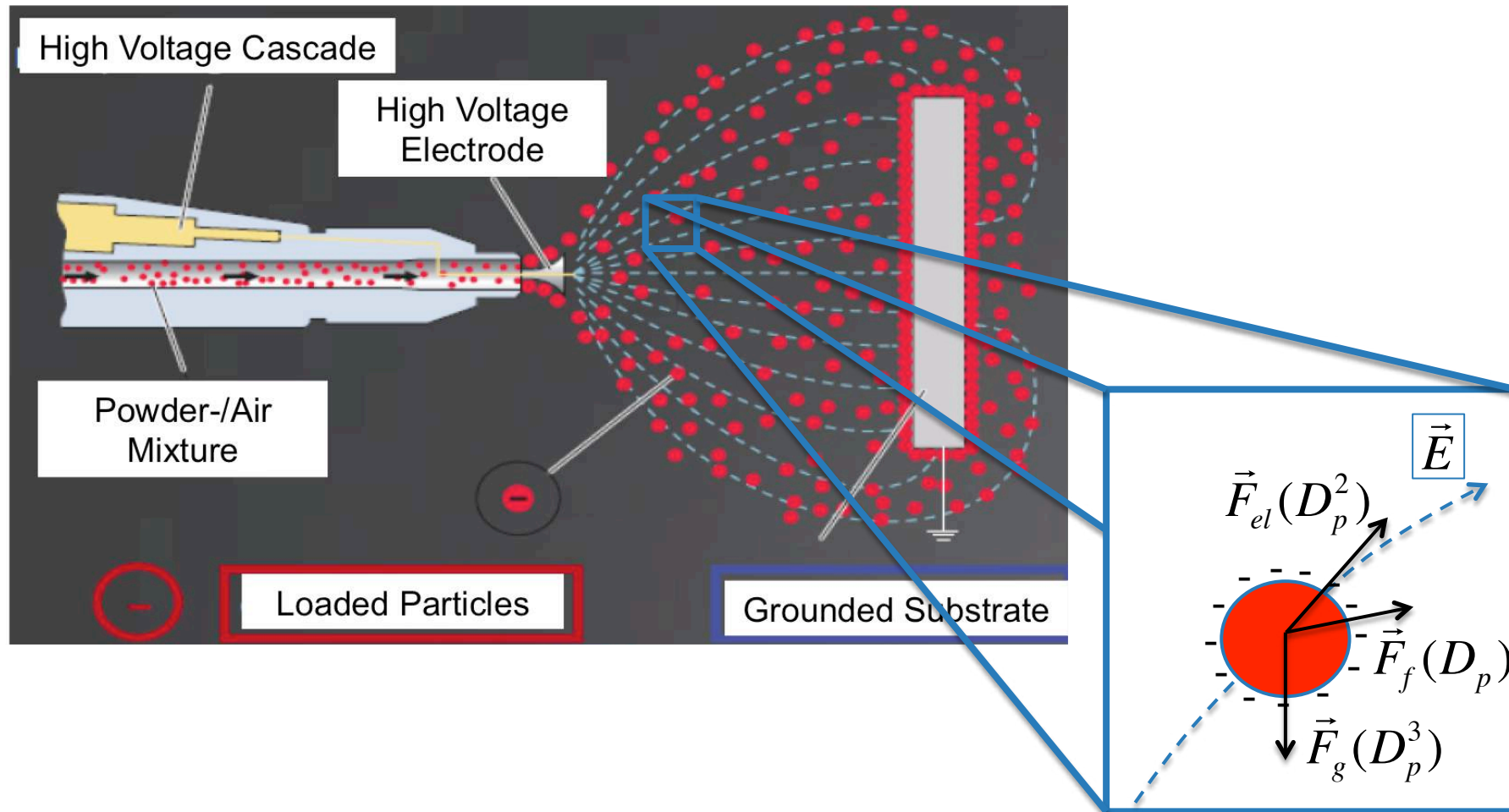


# 1. Overview & Introduction



# 1. Overview & Introduction

## Powder Coating: Flow, Particle-Dynamics, E-Static



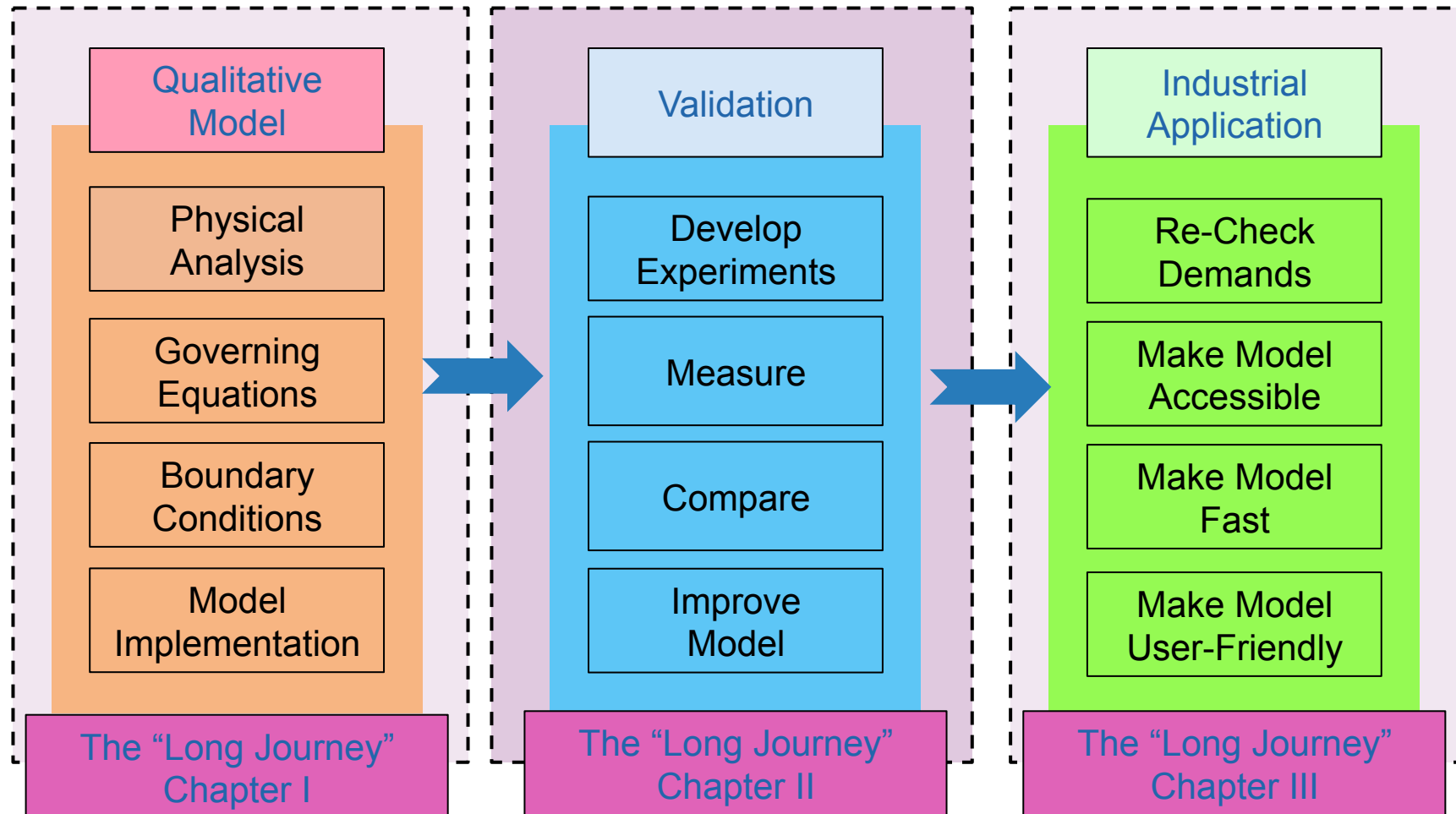
Acting Forces



Main Task?

Content

# 1. Overview & Introduction



## 2. Qualitative Modelling, Validation



# Content



# ICM 2007 - Manchester

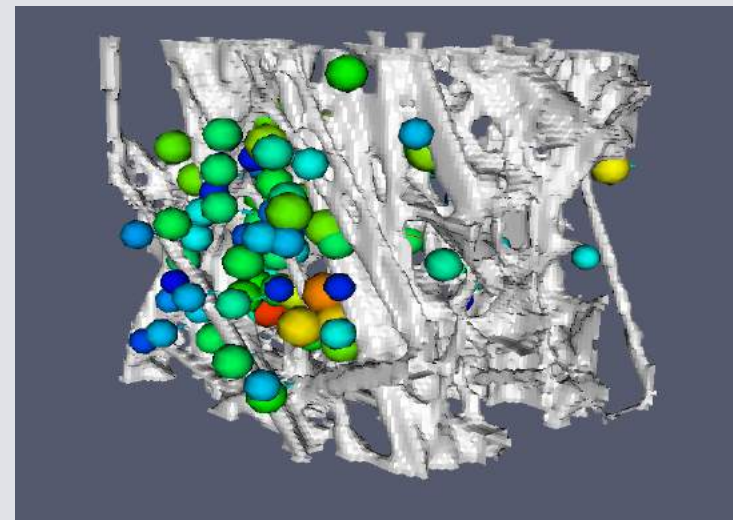
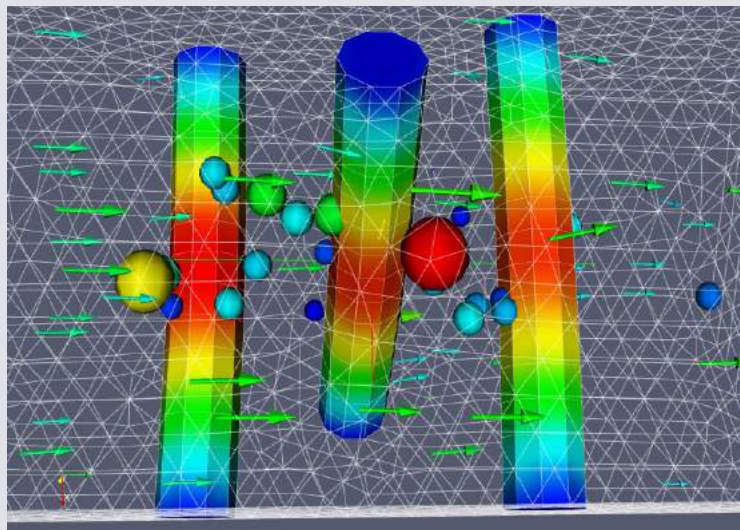
Zürcher Hochschule  
für Angewandte Wissenschaften

**zhaw** School of  
Engineering  
ICP Institute of  
Computational Physics



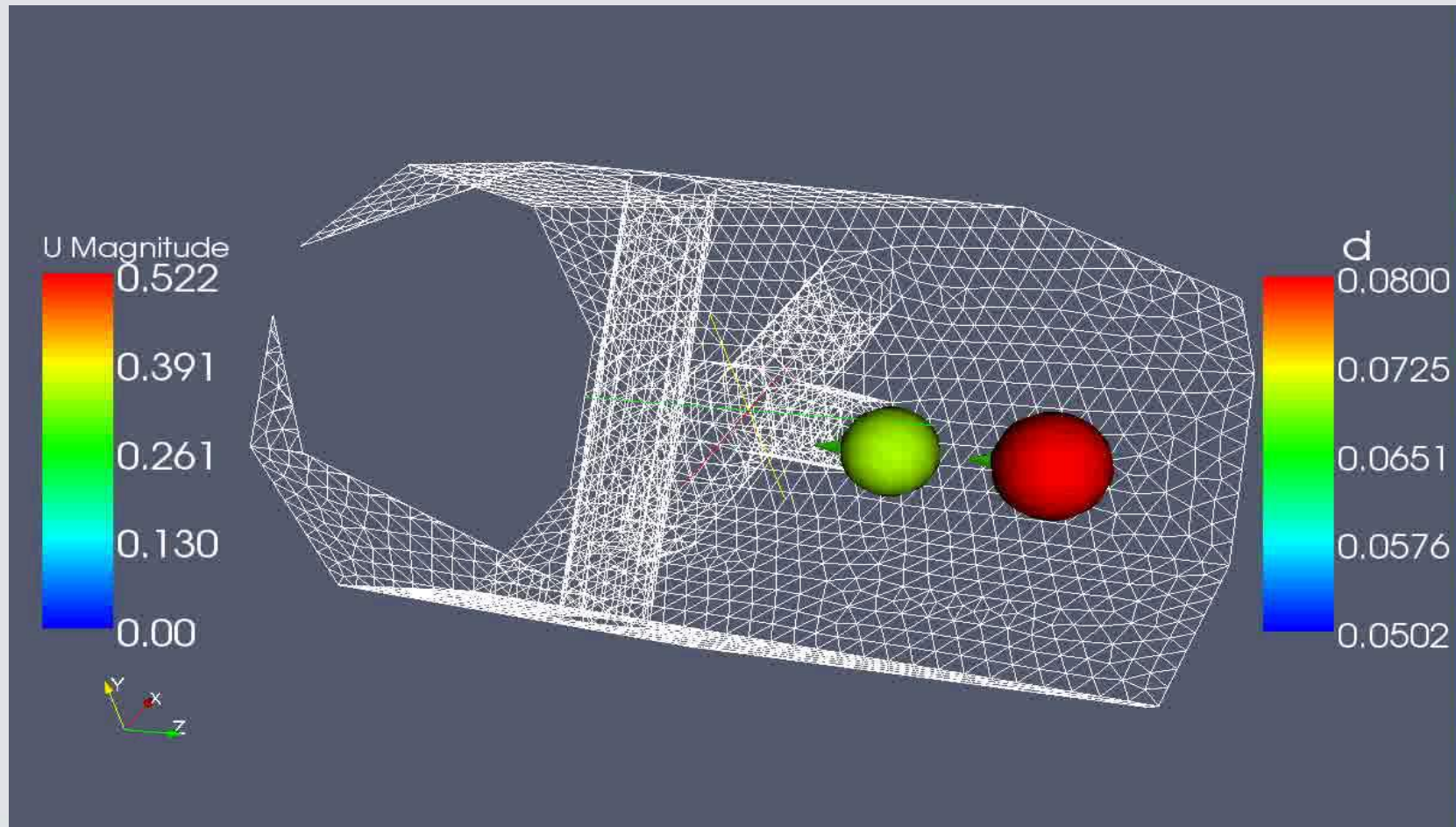
Source: <https://www.multiphysics.org/past-conferences>

# Particle filtration processes in deformable media



**Multiphysics Conference, Manchester, 12.12.- 14.12. 2007**  
**Gernot Boiger, Marianne Mataln**

## OpenFOAM: Euler - LaGrangian Solver – Blow Off Effect





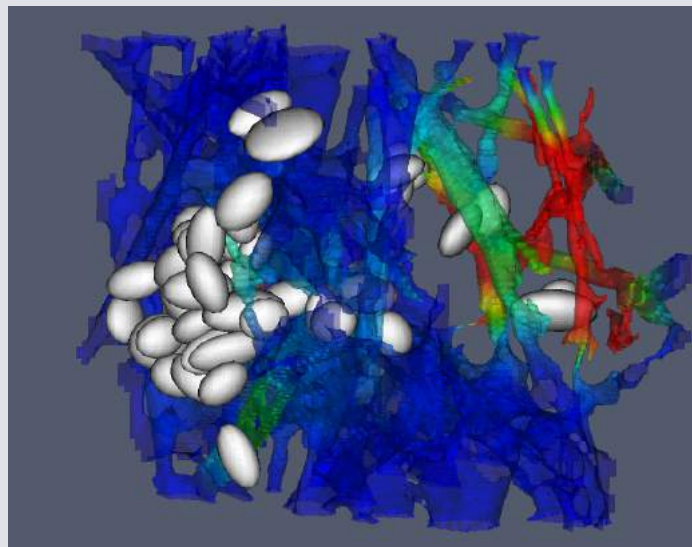
# ICM 2008 - Narvik



Sources: [multiphysics.org/past-conferences](http://multiphysics.org/past-conferences); [agoda.com](http://agoda.com);

# Simulation of Filtration Processes in Deformable media

## Part 3: Non-Spherical dirt particle modelling



**MultiPhysics, Narvik, 10.12.- 12.12. 2008**  
**Gernot Boiger, Marianne Mataln**

## Auxiliary Concepts:

### Pressure/Velocity Help Points:

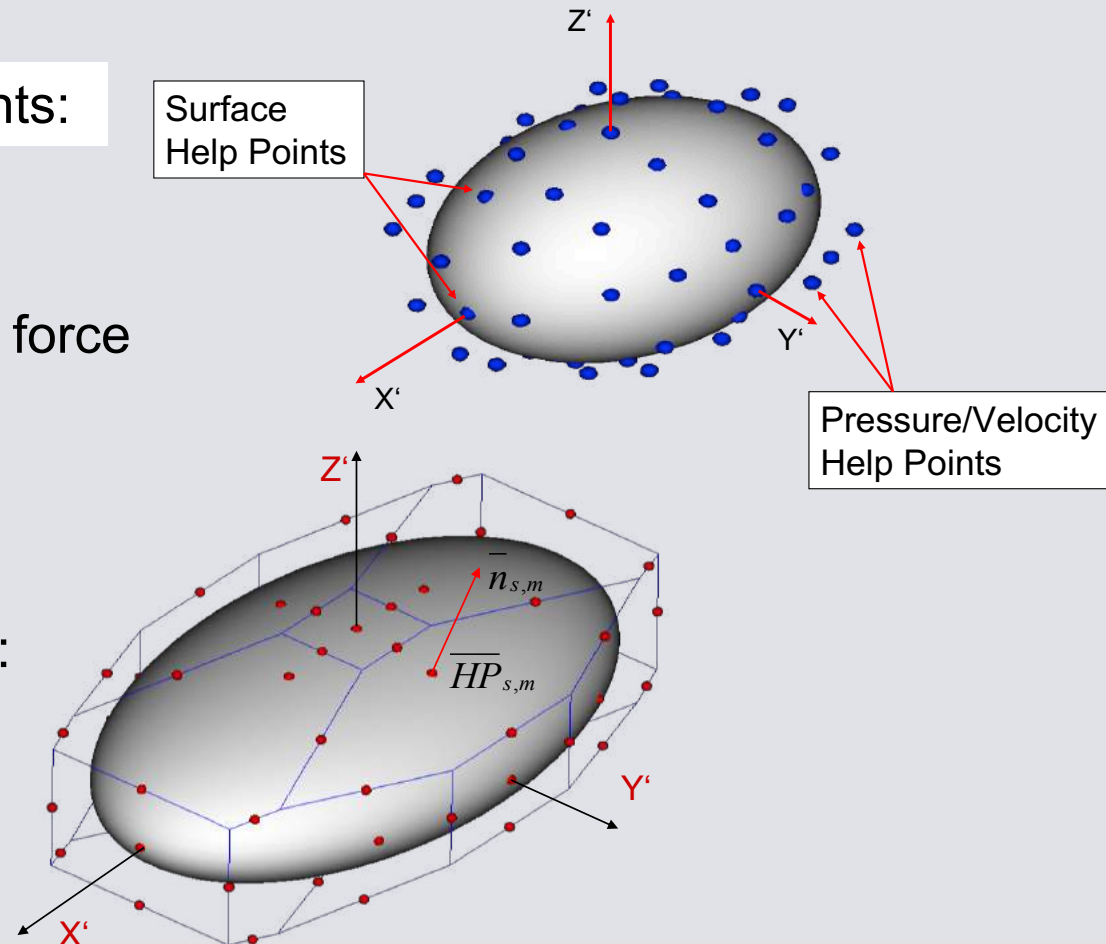
**66 Points** for detection of:

- relative fluid velocity
- acting pressure/shear force
- collisions

### Panel methode:

**18 Panels** for calculation of:

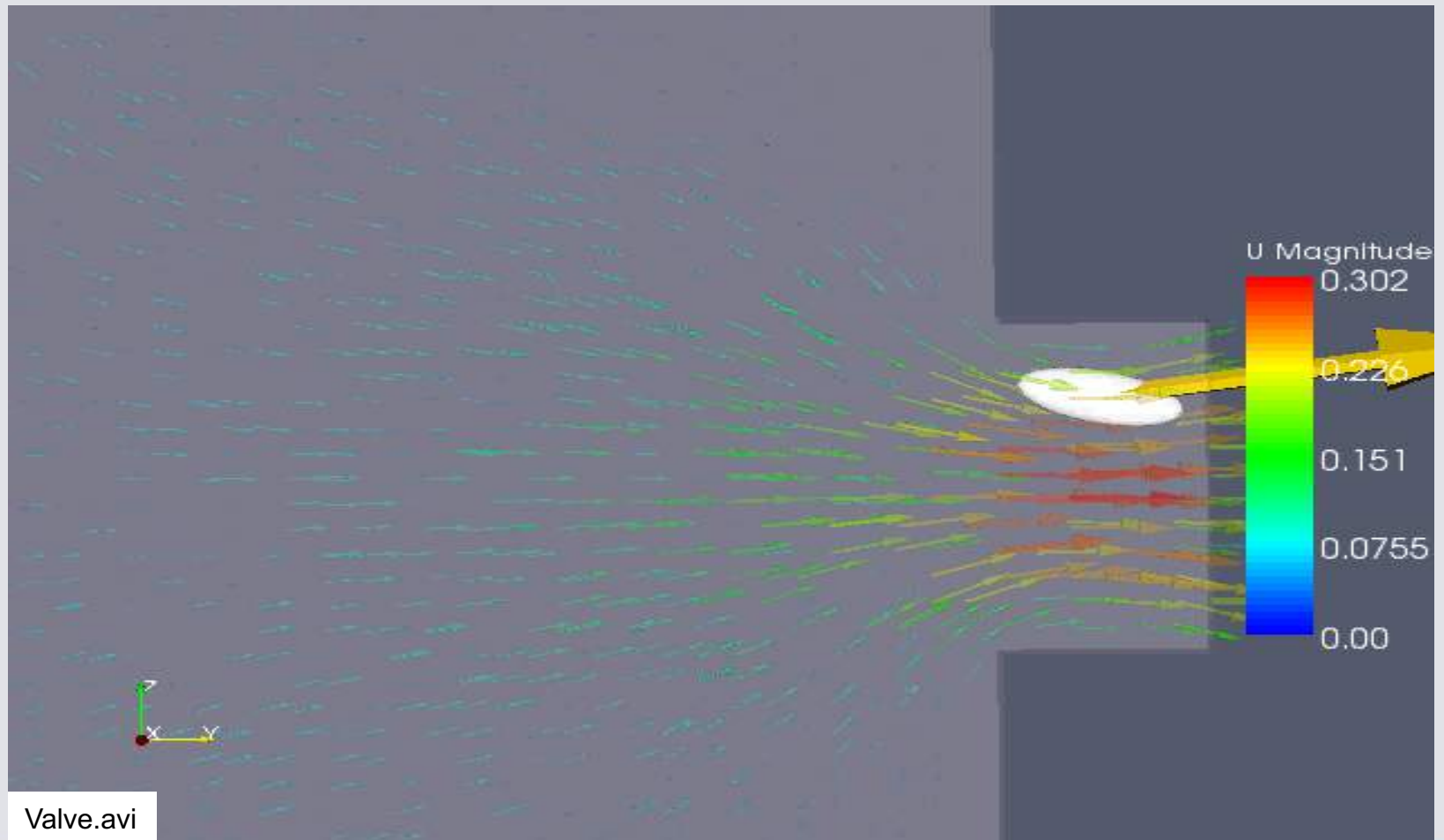
- local drag force
- rotational effects



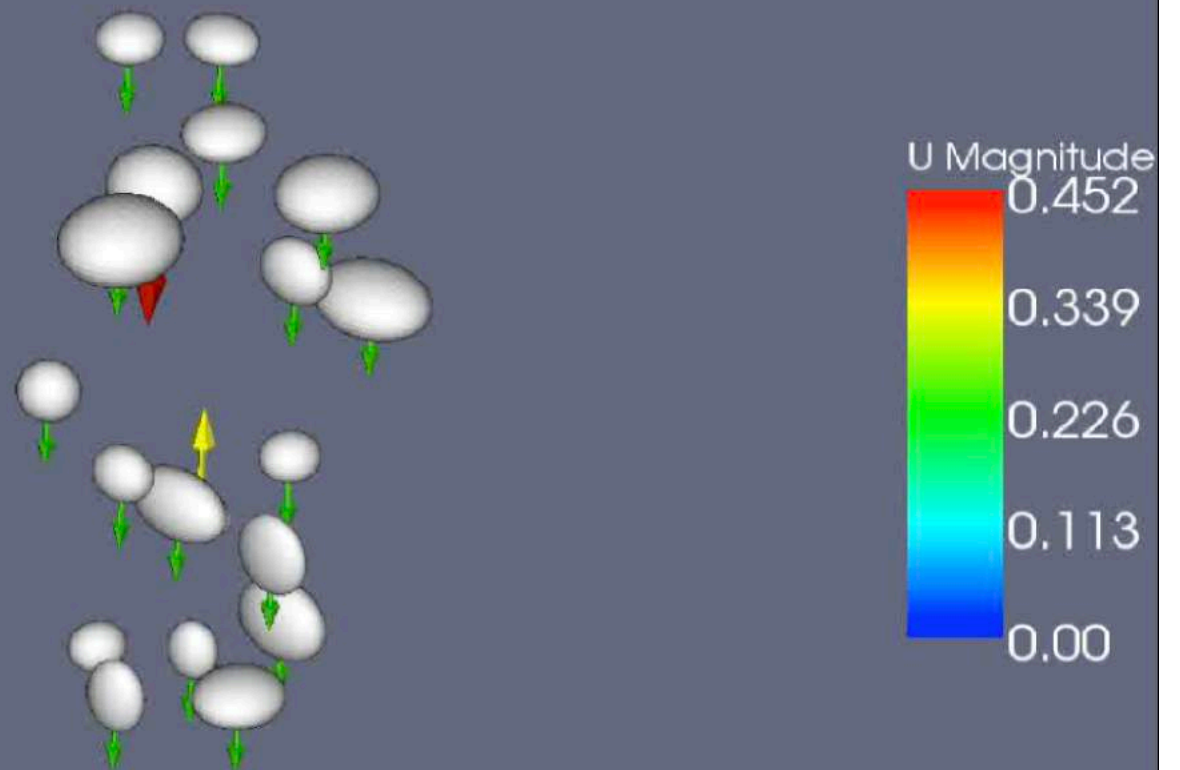


# ICM 2008 - Narvik

## Benchmark – Valve Effect

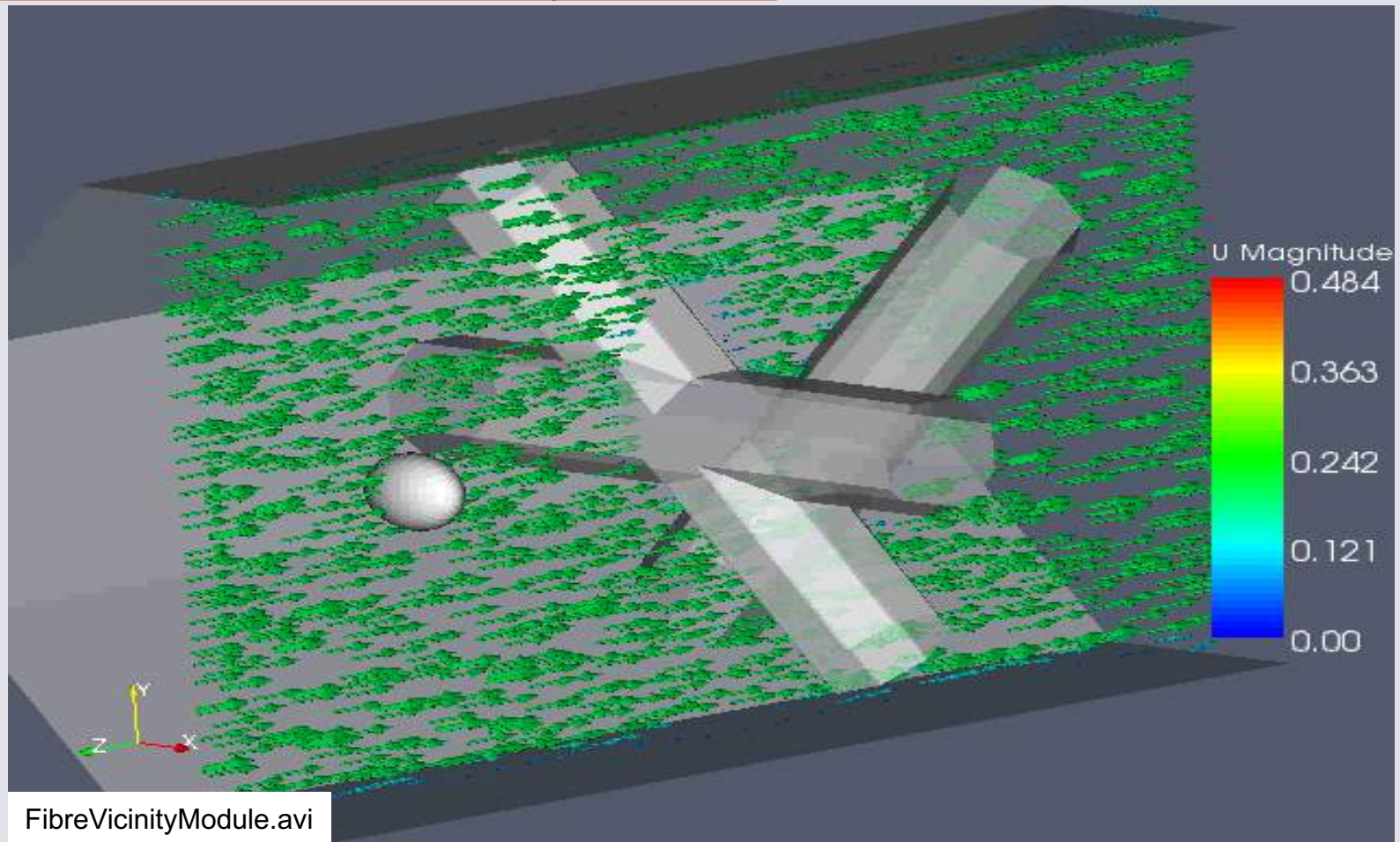


# ICM 2008 - Narvik



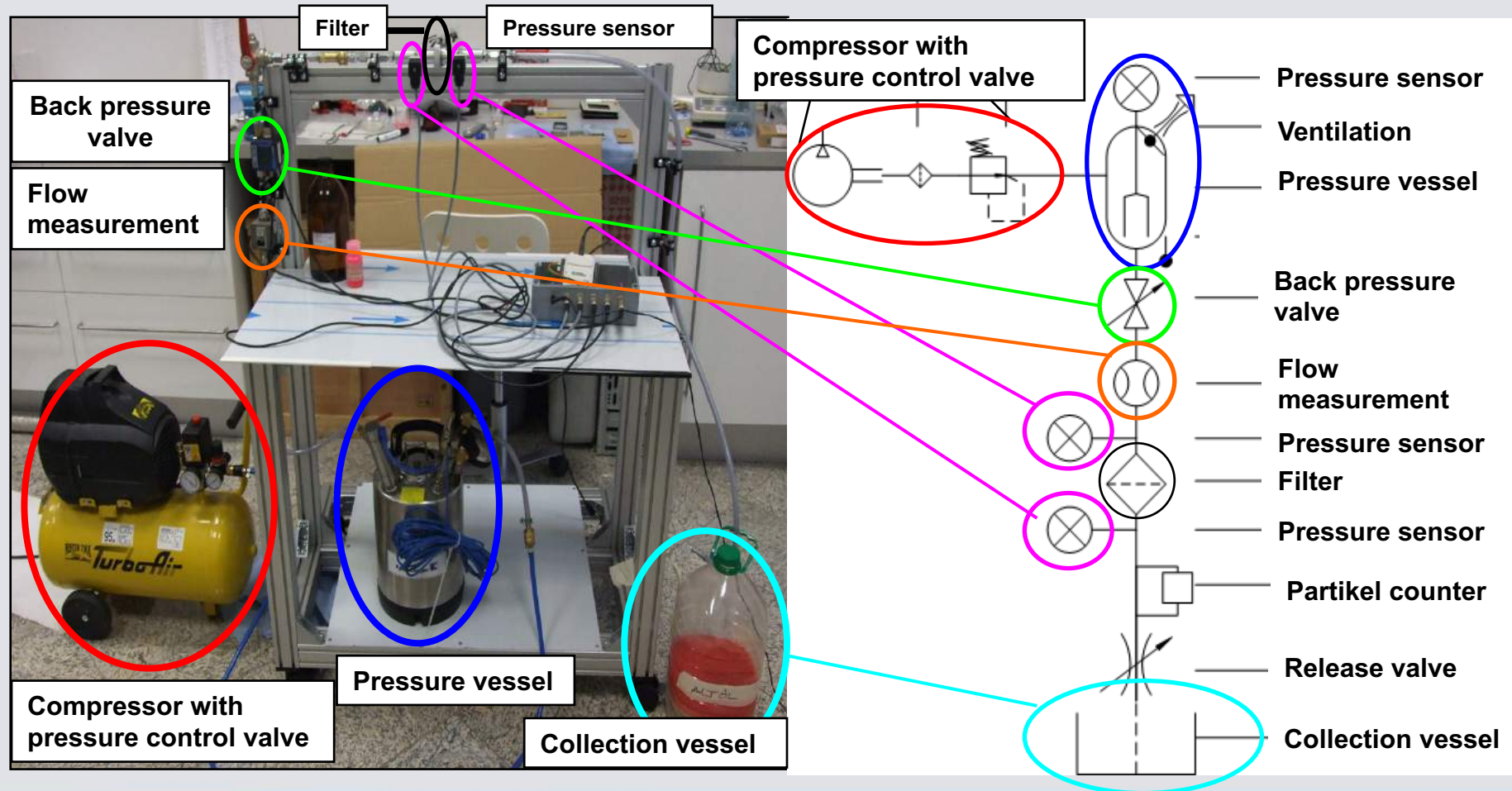
# ICM 2008 - Narvik

## Benchmark – Fibre Vicinity Module





## Oil/Fibre Test according to ISO 4548 -12



# ICM 2008 - Narvik

## Evaluation Facility: Sample holding device

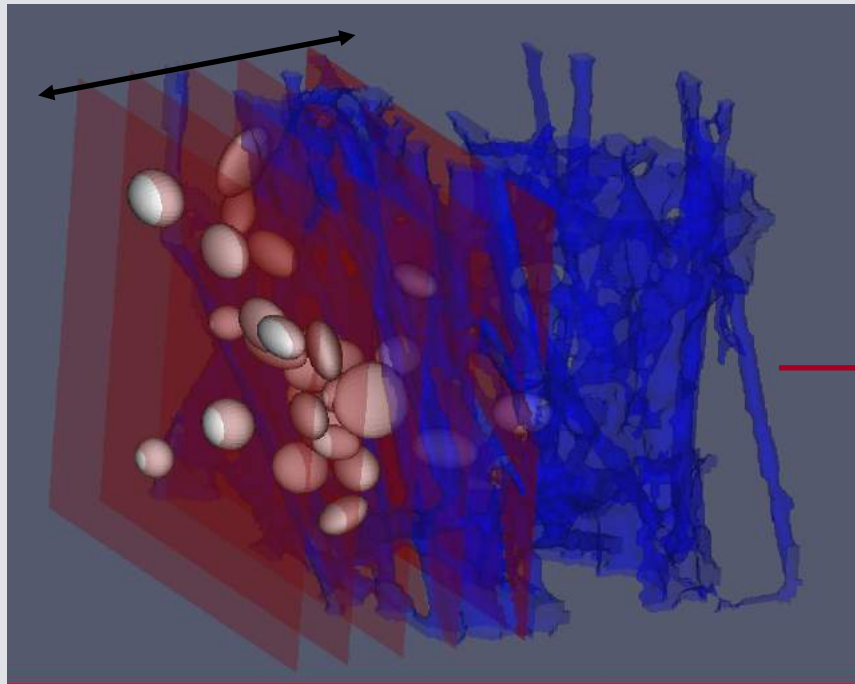


1. Sample holding device
2. PIV Cam
3. DriveSet
4. Laser

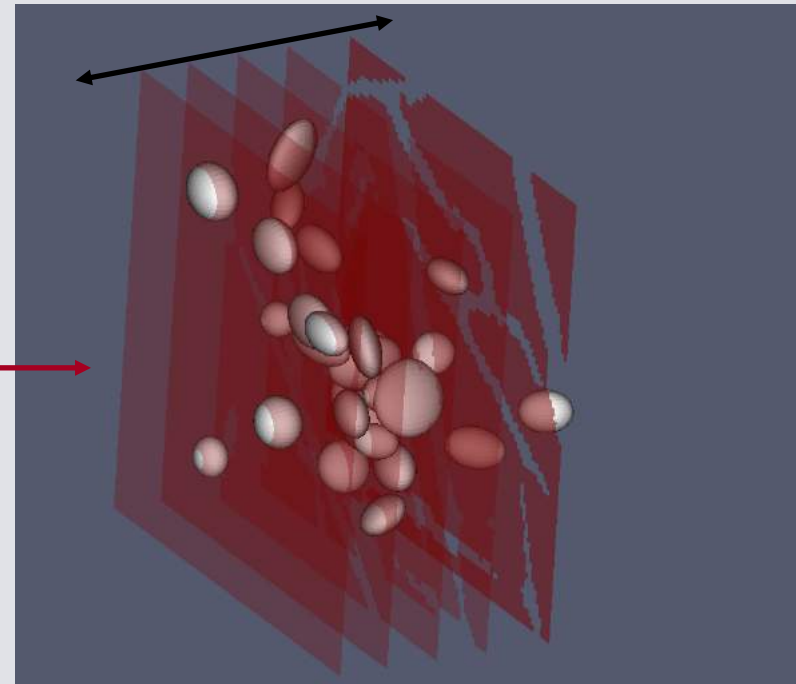


## Principle of 3D Macroscopy

Focal Plane is moved through Fibre

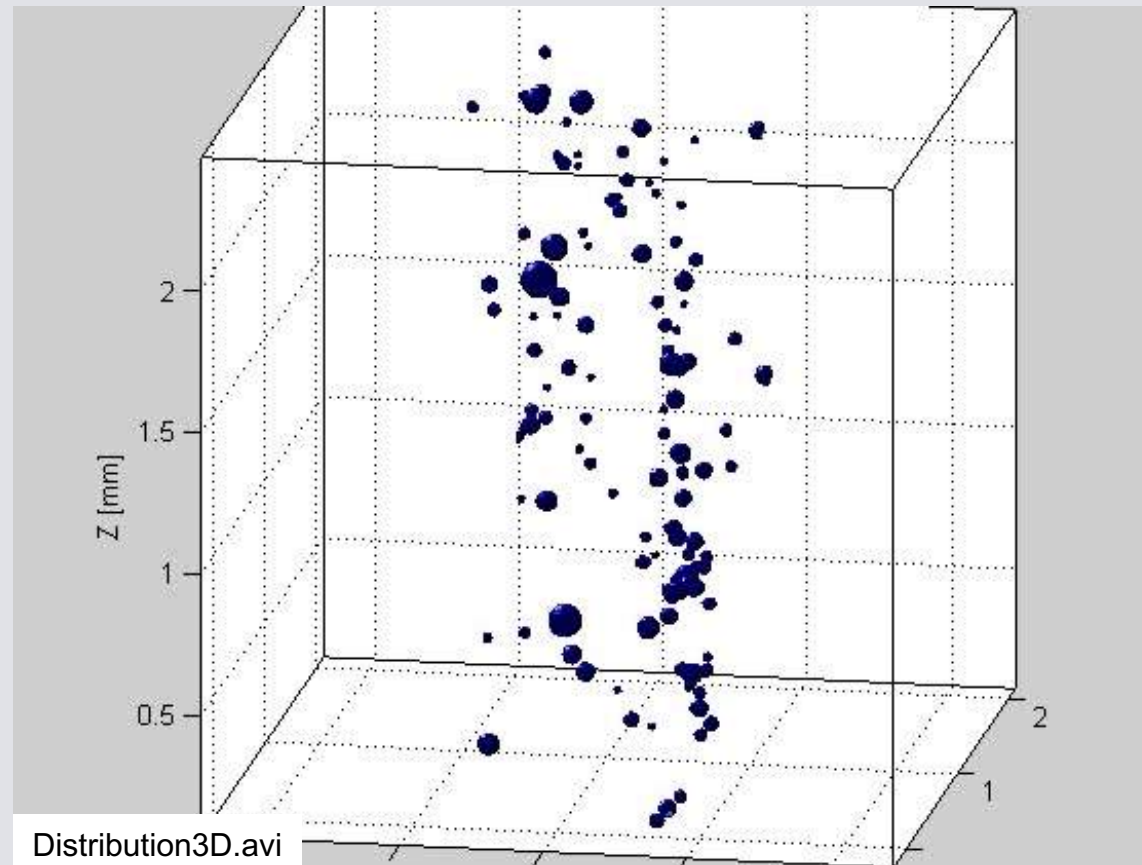


Particles entangled in  
Fibre structure



Reconstruction of  
Particle Distribution

## Evaluation Results: Matlab Evaluation Algorithm



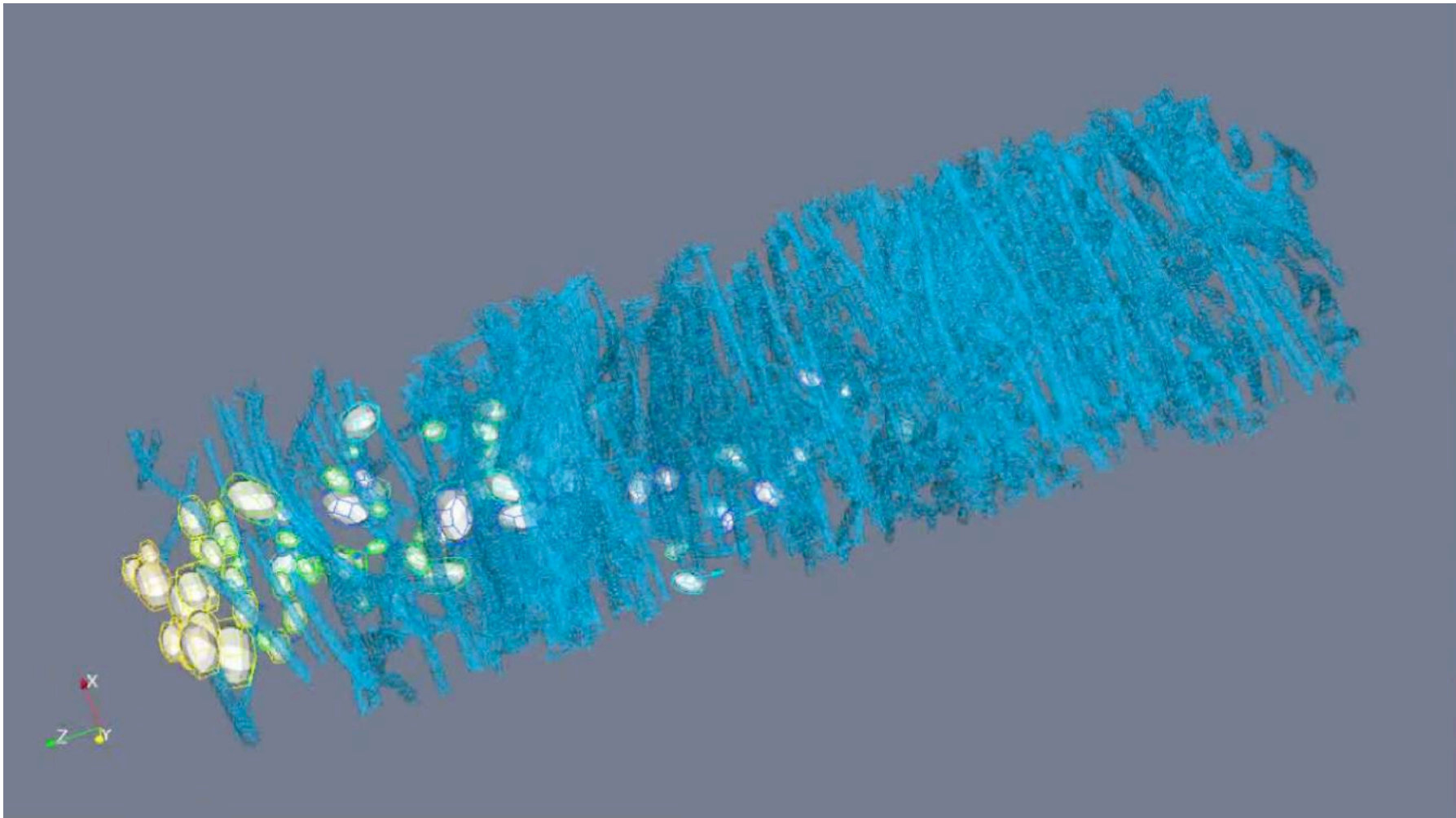
3D Reconstruction of Particle Distribution in Fibre Sample



# Qualitative Model - 2010

Zürcher Hochschule  
für Angewandte Wissenschaften

**zhaw** School of  
Engineering  
ICP Institute of  
Computational Physics



Boiger,G.; Mataln,M.; Brandstätter,W., 2009. Simulation of Particle Filtration Processes in Deformable Media, Part 3.1: Basic concepts and particle-fluid force implementation of a non-spherical dirt particle solver, (2010), Int.Journal of Multiphysics. 3(4), pp. 407-232(26). DOI: 10.1260/1750-9548.3.4.407.

# ICM 2013 - Amsterdam

Zürcher Hochschule  
für Angewandte Wissenschaften

**zhaw** School of Engineering  
ICP Institute of Computational Physics



Source: <https://www.multiphysics.org/past-conferences>

## Thermo Fluid- Dynamic Model of Wood Particle Gasification and Combustion Processes

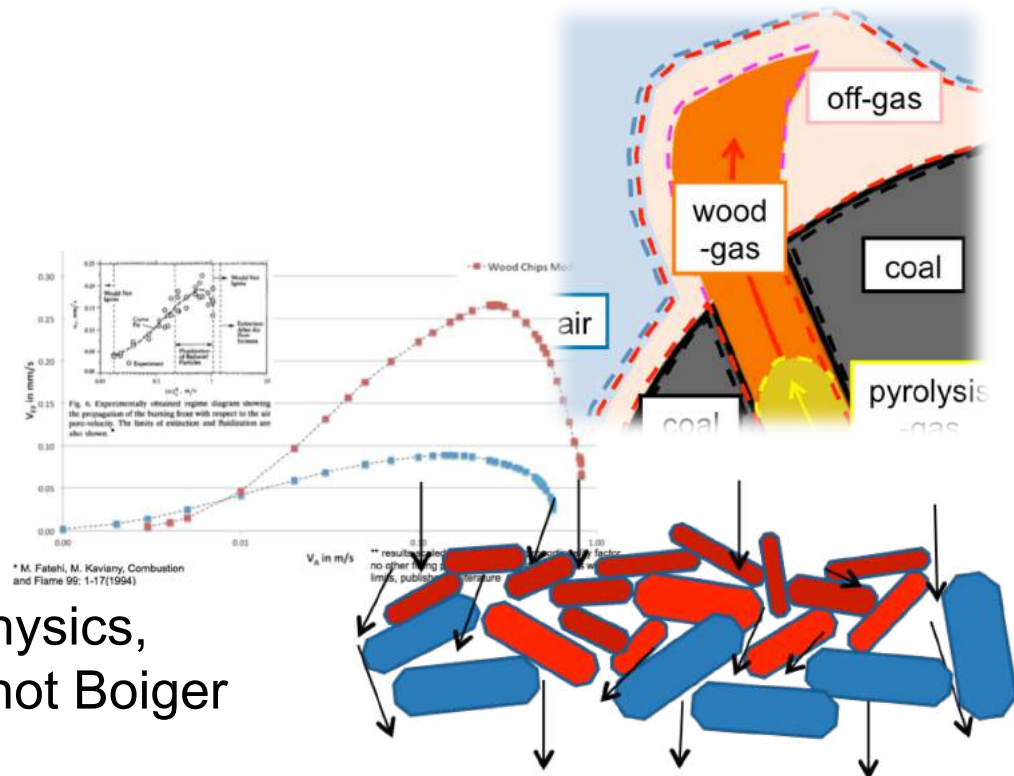
### 1<sup>st</sup> step:

Fully Featured 1D-Solver for  
Particle Gasification

### 2<sup>nd</sup> step:

Experimental Validation

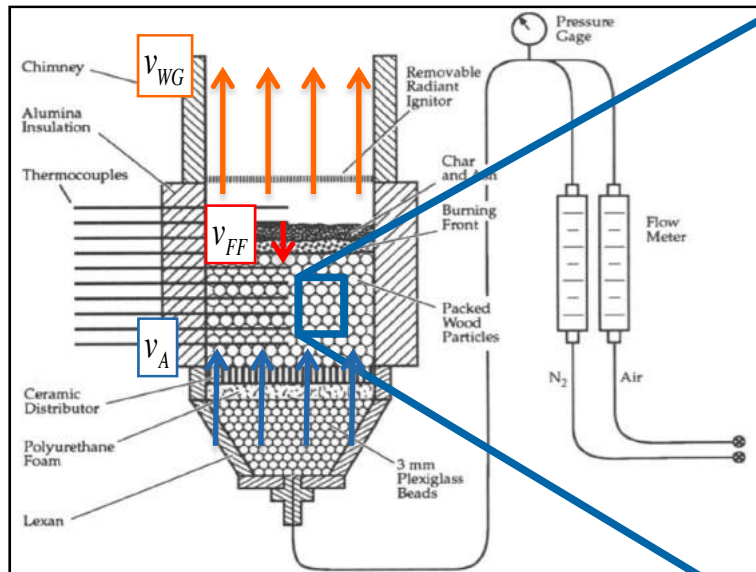
International Conference of Multiphysics,  
Amsterdam, December 2013, Gernot Boiger



# ICM 2013 - Amsterdam

## Model Scale: Packed Bed-/ Particle Level

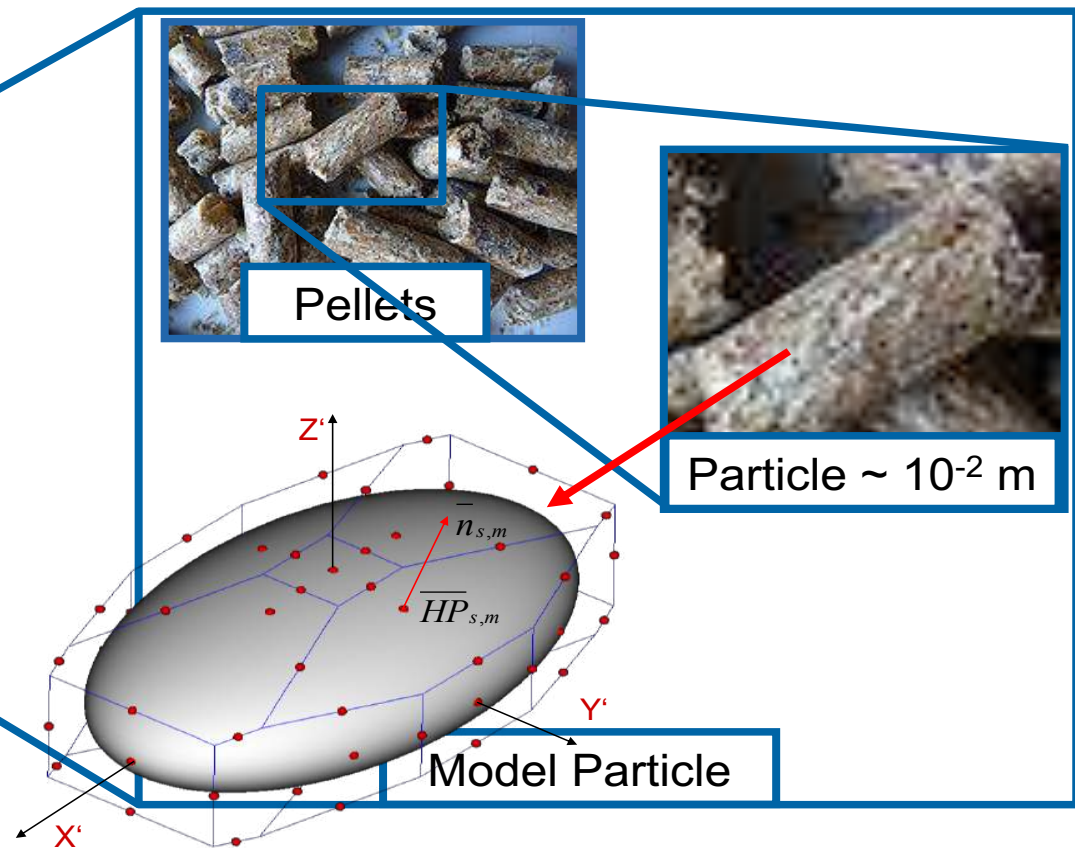
### Counter – Current “Up-Draft” Wood Gasifier



Source: M. Fatehi, M. Kaviany, Combustion and Flame 99: 1-17(1994)

07.12.22, G. Boiger, ICP, ZHAW Winterthur  
Zürcher Fachhochschule

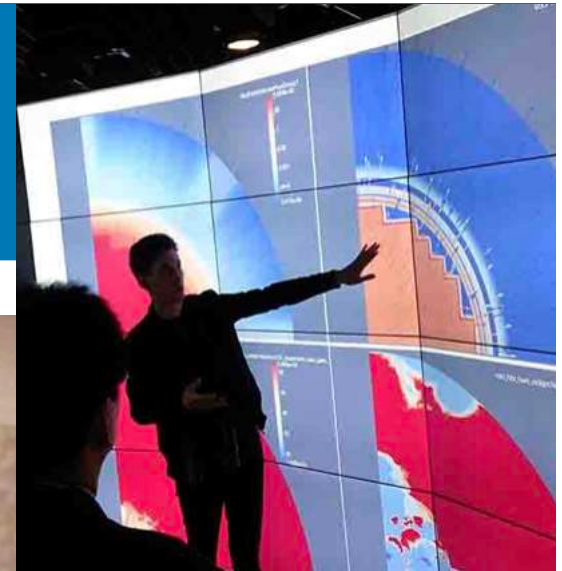
### Hybrid Bulk- Particle Model



Boiger, G., 2015. System Dynamic modelling approach for resolving the thermo- chemistry of wood gasification processes, (2015), Int. Journal of Multiphysics. 9(2), pp. 137-155(19). DOI: 10.21152/1750-9548.10.2.177.



# ICM 2015 - London



Source: <https://www.multiphysics.org/past-conferences>

# ICM 2015 - London

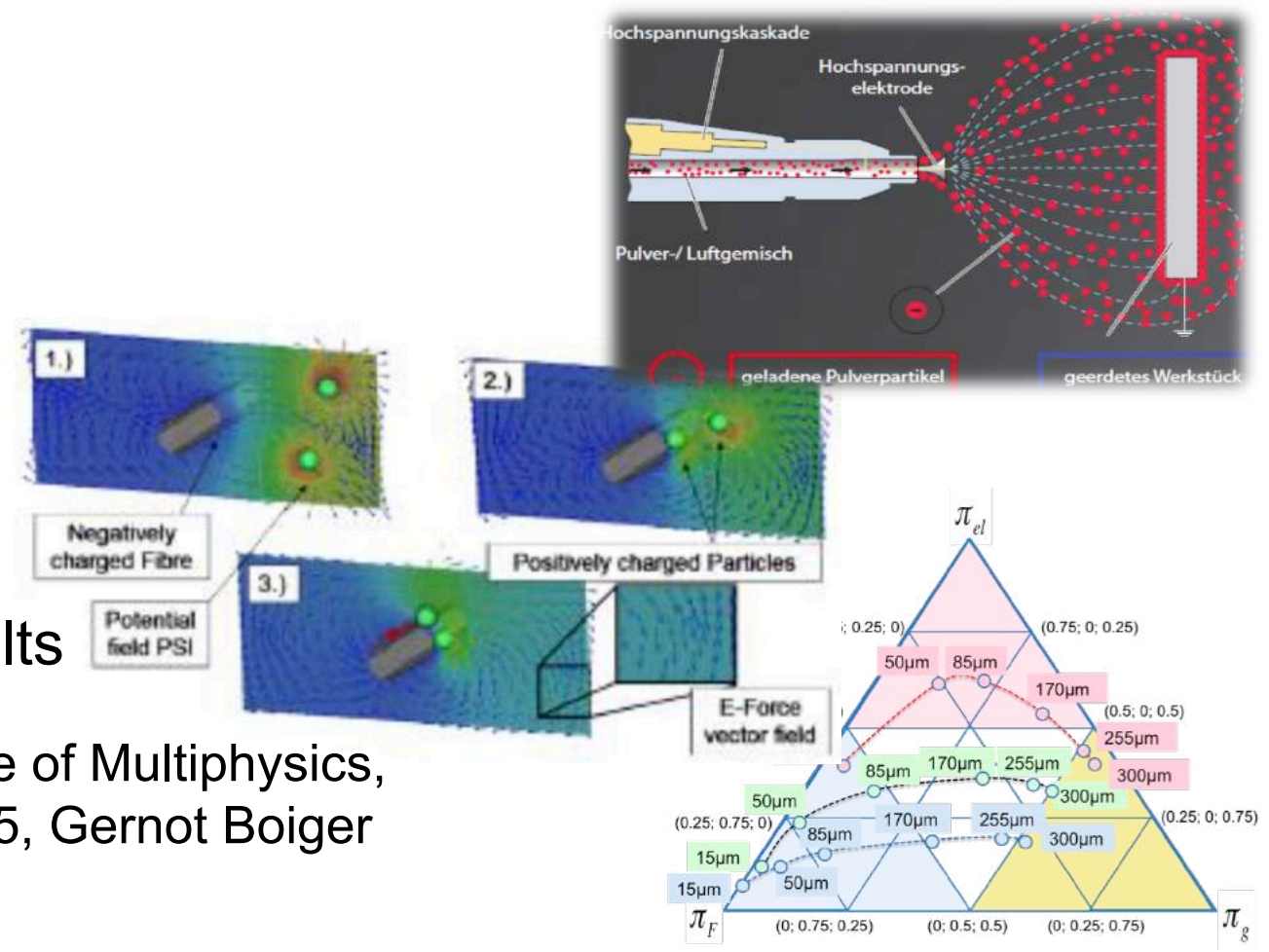
## OpenFoam based Modelling of 3D LaGrangian Particle Motion and Deposition within E-Static Fields

**1<sup>st</sup> step:**  
 Powder Coating

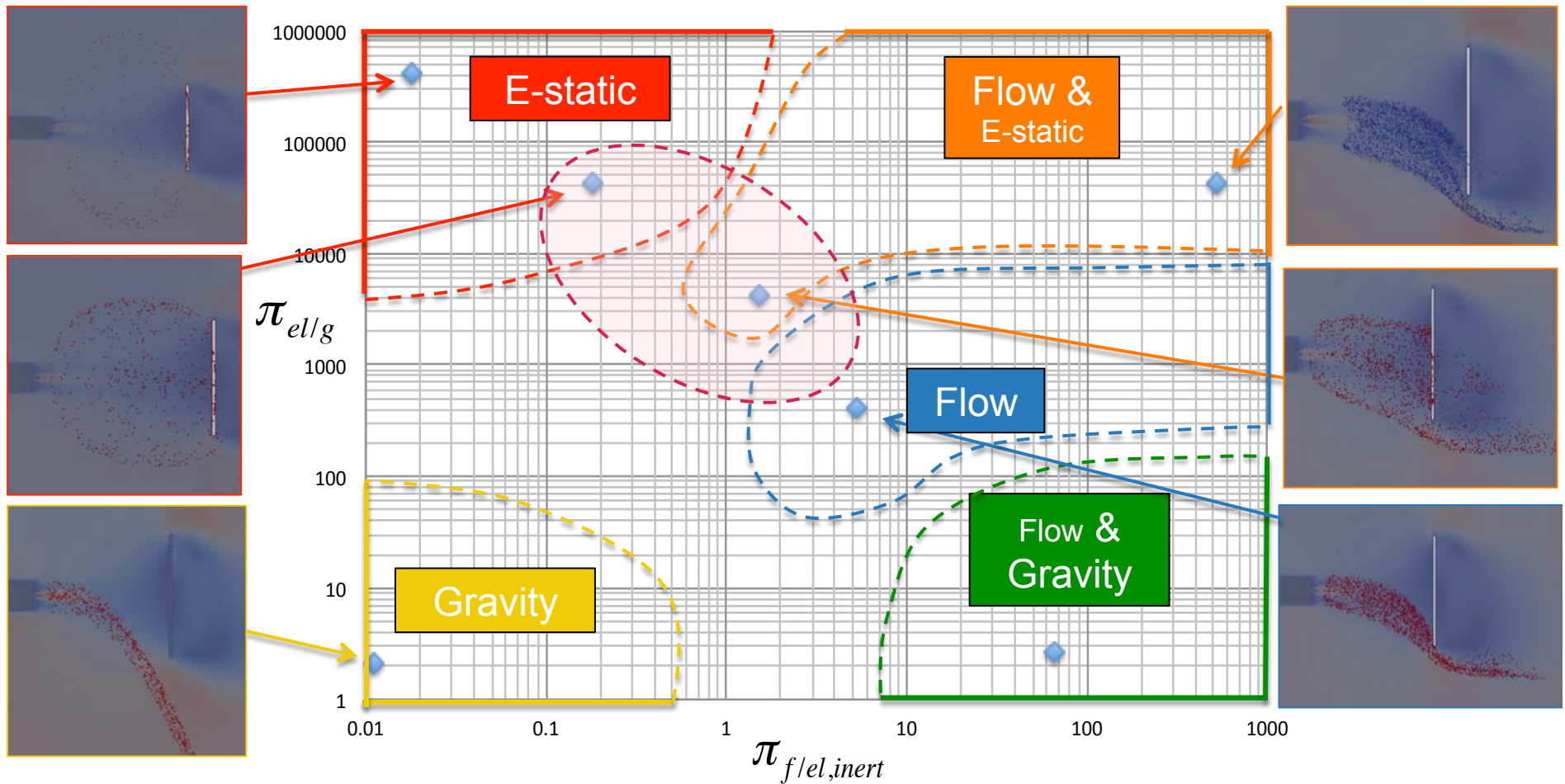
**2<sup>nd</sup> step:**  
 The 3D Model

**3<sup>rd</sup> step:**  
 Validation and Results

International Conference of Multiphysics,  
 London, December 2015, Gernot Boiger



# ICM 2015 - London

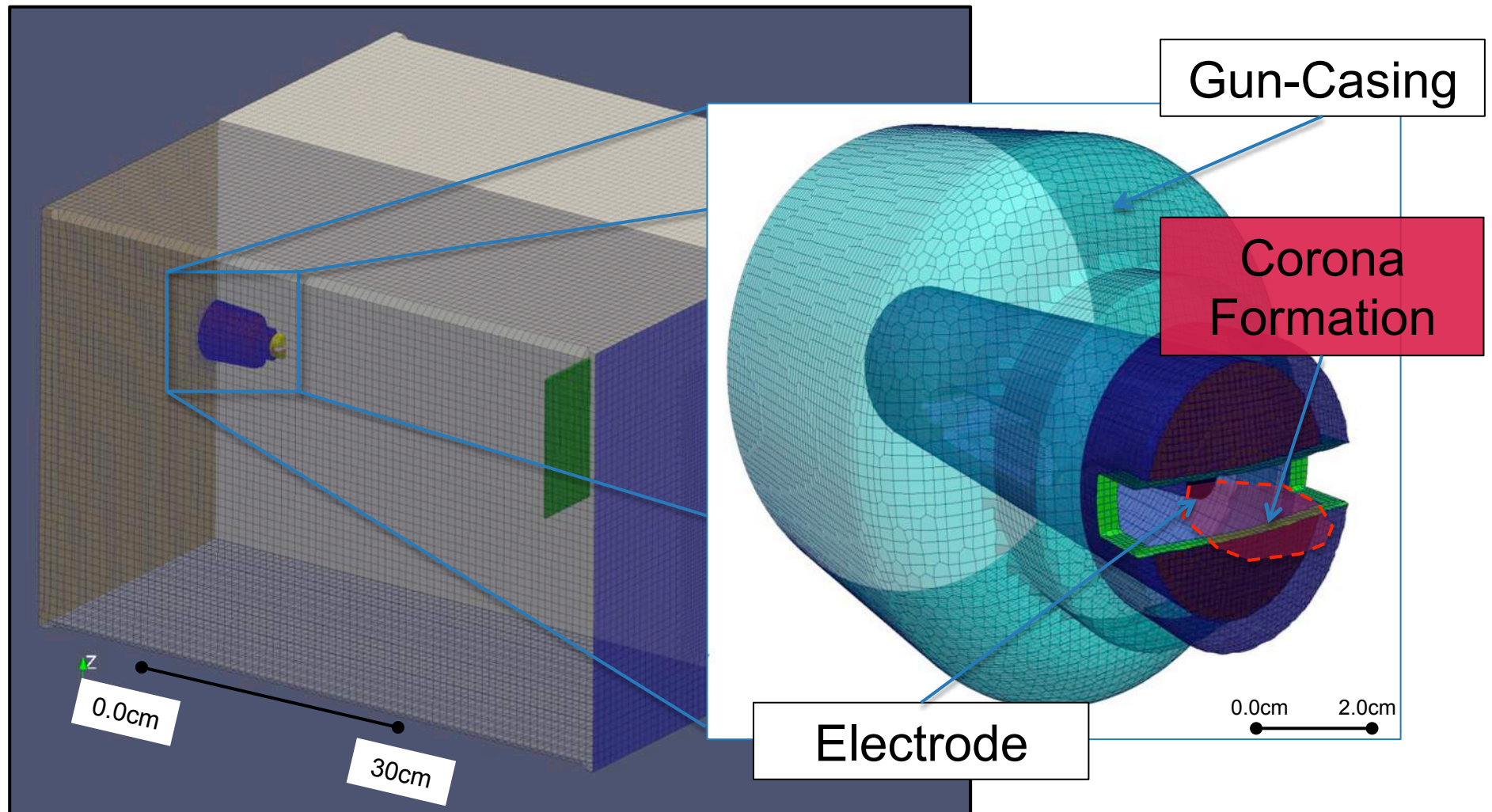


$\pi_{el,g}$  : Ratio of E-Static to Gravit

$\pi_{f,el,inert}$  : Ratio of Viscosity to E-Static \* Inertia



## Modeling the Geometry & FV Meshing





## Modeling Particle Dynamics: Particle Momentum Equation

$$\frac{\partial^2 \vec{x}_p}{\partial t^2} = \frac{\vec{U}_{FP}}{\tau_p} + \frac{\rho_p - \rho_F}{\rho_p} * \vec{g} + \frac{q_p D_p^2 \pi}{m_p} * \left( \vec{E} + \frac{D_p^2 \pi}{4\epsilon} \nabla \rho_c \right)$$

Aerodynamic Coupling  
to Flow Field

Gravity  
Field

E-Static  
Field

Electric Particle-  
Particle Interaction

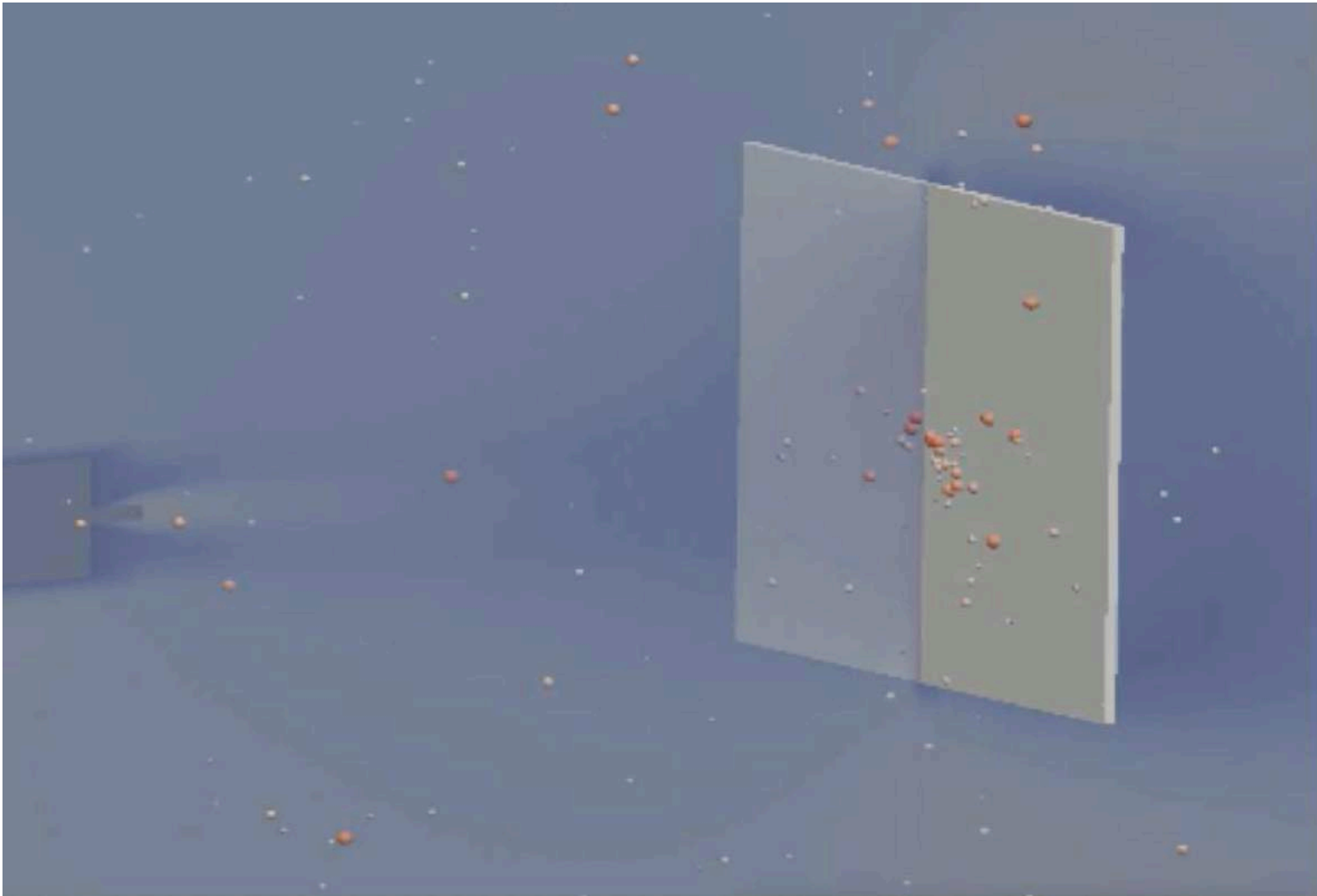
$\vec{U}_{FP}$  (m/s) ... Particle - Flow  
Relative Velocity

$q_p$  (C/m<sup>2</sup>) ... Particle Surface Charge

$\vec{E}$  (N/C) ... Electric Field

$\tau_p$  (Re<sub>p</sub>)(s) ... Particle Relaxation Time

# ICM 2015 - London



# ICM 2016 – Winterthur/Zurich



Source: <https://www.multiphysics.org/past-conferences>

## Multiphysics 2016 Electrostatic-Powder-Spray-Coat

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Bachelor in Mechanical Engineering  
Institute of Computational Physics  
Zürich University of Applied Sciences (ZHAW)  
Technikumstrasse 15, 8404 - Winterthur, Zurich - CH - Switzerland  
stephan.weilenmann, gernot.boiger, (@zhaw.ch)



**Abstract**  
Electrostatic powder spray coating is a widely used method in nowadays industrial applications to improve surface properties - by adding a protective layer onto the whole surface of a mechanically favourable bulk material. An effective transient numerical solver under the application of physical laws in combination with the finite volume method approach could be developed and validated. Design-concept enhancements have been proposed and evaluated. The key factors for the evaluation of the different powder spray particle concepts are the transfer efficiency  $TE$ , the partial coating volume difference  $PCVD$  and the relative standard volume deviation  $RSVD$  of each front-backside.

**1. Introduction**  
MODELLING of the electrostatic powder spray coating is a complex process including knowledge about aerodynamics, electrostatics and particle charge, motion. It has been observed that the two most common nozzle shapes produce different distributions on substrates. The fan nozzle applies a almost Gaussian like distribution whereas the difuser nozzle produces a doughnut distribution. This indicates that the fan nozzle shape plays a significant role in the coating quality. The advantage of EPSC to non-electrostatic coating processes is that the whole substrate can be coated at once. On the other hand due to sharp corners a so called shadow frame occurs whereby the thickness of the substrate surface along the corner compared to the distal is thicker.

**2. simulation Model**  
The new simulations build up on a previous validation of the spray-particle- $\phi$  simulation with the in-house experimental setup. Therefore a reduced coating chamber with four different powder-spray-plats and an aluminium-substrate plate as shown in fig.1 were initialised under common operating conditions.

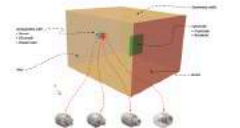


Figure 1: reduced coating chamber model with boundary particles and nozzle-design concepts. The four nozzle concepts (I) fan nozzle, (II) opt. fan nozzle, (III) elliptical nozzle and (IV) horned nozzle are shown from left to right respectively.

The ideas behind the design-concept (III) are to divide the particle spray by destination back-frontside and to condense the spray cloud by using an elliptical shape. For the design-concept (IV) a rotating injection canal and nozzle has been introduced. Through centrifugal forces the different particle sizes get reorganized. The injection canal diameter shrinks with proceeding length until the circular nozzle-opening where the shape separates to produce a cone cloud.

**3. mathematical Model**  
Air flow is modelled by the momentum-equation (1) under the assumption of incompressible fluid motion  $Ma < 0.3$  including the gravitational field

$$\rho \frac{d\vec{v}}{dt} + \rho(\vec{v} \cdot \nabla) \vec{v} = -\nabla p + \mu \nabla^2 \vec{v} + \rho \vec{g}$$

$\vec{v}$  is the air velocity vector,  $\vec{g}$  the gravitational field constant,  $\mu$  the air viscosity and  $\rho$  the air density.

The electric field (2) has been modelled by Maxwell's First Law

$$\nabla^2 \phi = -\frac{\rho_f}{\epsilon_0 \epsilon_r}$$

$\phi$  electric potential,  $\rho_f$  surface charge, and  $\epsilon_r$  relative permittivity. The trajectory of the particles have been modelled by the use of the Lagrangian Approach in which Newton's Second Law states the particle force (3) is equal to the sum of the external forces (4)

$$\vec{F}_p = m_p \frac{d\vec{v}_p}{dt} = \sum \vec{F}$$

$$\sum \vec{F} = \vec{F}_{Drag} + \vec{F}_{Gravity} + \vec{F}_{Electrostatic}$$

$\vec{F}_{Drag}$  drag force on particle,  $\vec{F}_{Gravity}$  gravity acting on particle, and  $\vec{F}_{Electrostatic}$  electrostatic field on particle

**4. Results and Discussion**  
Three factors are analysed and discussed to quantify the coating quality. First the transfer efficiency  $TE$  (ideally 1) states the ratio between the adhering to the injected particles.

$$TE = \frac{M_{adhering}}{M_{injected}}$$

Second factor partial coating volume difference  $PCVD$  (ideally 0.5) considers the coating volume difference to total volume of front-backside

$$PCVD = \frac{V_{frontside} - V_{backside}}{V_{frontside} + V_{backside}}$$

The third relative standard volume deviation  $RSVD$  compares the ratio of standard deviation to the mean of the particle volume (ideally 0) under a normal distribution  $N(\mu, \sigma^2)$

$$RSVD = \frac{\sigma}{\mu}$$


Figure 2: Transfer efficiency of (I-IV) depending on applied voltage.

**4.2 partial coating volume difference**  
For rising voltage a decay in PCVD towards the ideal PCVD of about 0.5 is visible. Two nozzle shapes cross or get close to the value of 0.5 (N) at 100kV (N) at 70kV (N) III shows poor front-backside particle division.

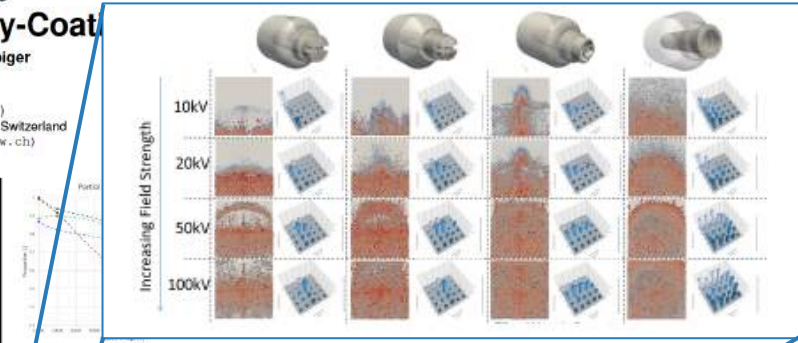


Figure 3: Partial coating volume  $PCVD$  of (I-IV) depending on applied voltage.

**4.3 Particle distribution**  
On both front and backside, a rise in the coating volume and the particle surface covering under amplification of the applied voltage is recognizable.

**4.3.1 Frontside**  
Fig. 4 shows the influence of gravity and the decentralization of the spray focus center at [0-50kV]. At 100kV most of the surface covered and the local spray point lies within the plate (prior area whereby N) shows lowest performance.

Figure 4: Frontside volume comparison between the different nozzle design concepts under increasing  $\Delta\phi$ .

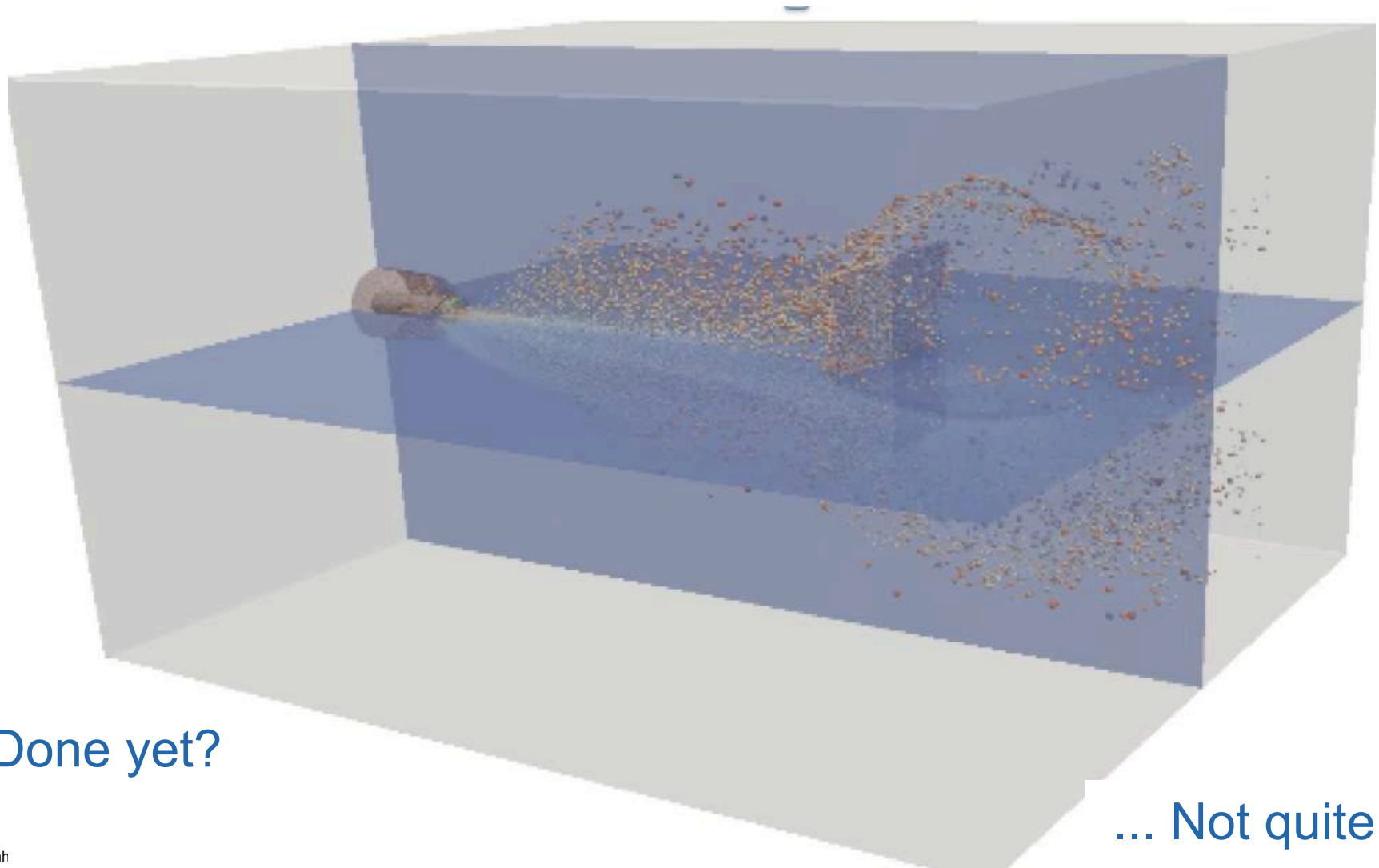
**4.3.2 Backside**  
In fig. 5 the influence of gravity on the spray cloud is visible in the whole voltage range. The shadow frame occurs in all cases from 20kV or upwards whereby denser coating areas in the lower half of the plate are noticeable.

Figure 5: Backside volume comparison between the different nozzle design concepts under increasing  $\Delta\phi$ .

**5. Conclusion**  
The new concepts show improvements in both efficiency and coating distribution. A rotating injection canal speeds up the particle velocity and hence can be operated at lower operation voltages. On the other hand, the partial coating volume difference is only improved in (N/V). With a 2-D Geometry-Optimization Algorithm further enhancements could be achieved in PCVD-factors.



# ICM 2016 - Winterthur



Done yet?

... Not quite!

# Validation Experiments - 2016

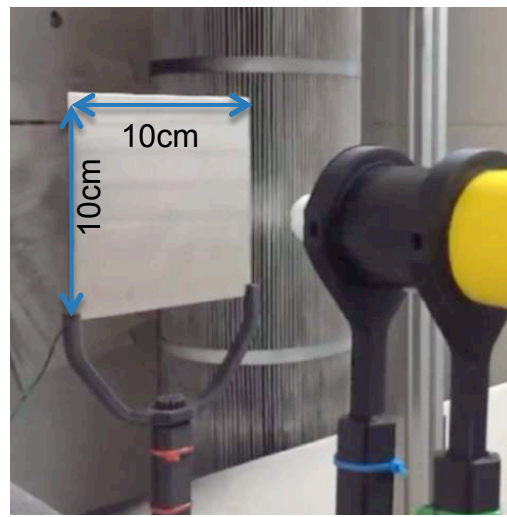
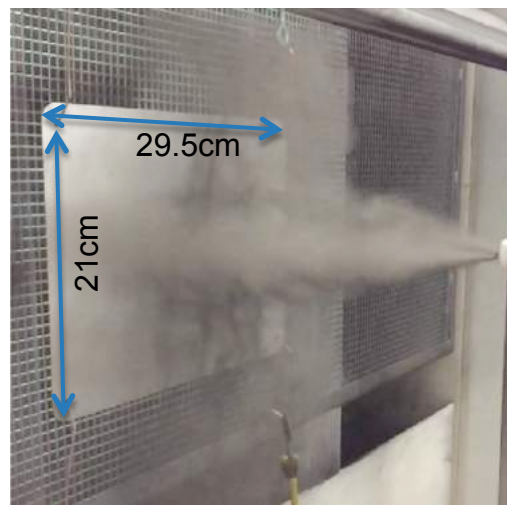
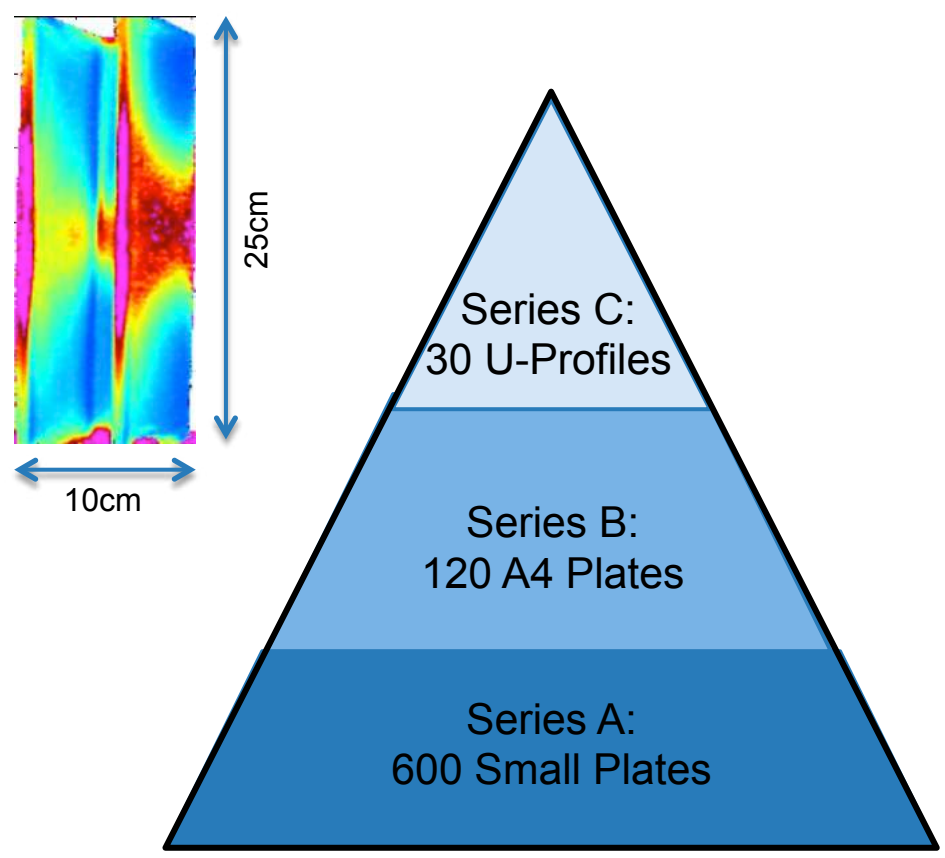
## Coating Lab at ZHAW:



Coating Experiment  
ZHAW Winterthur

# Validation Scheme - 2016

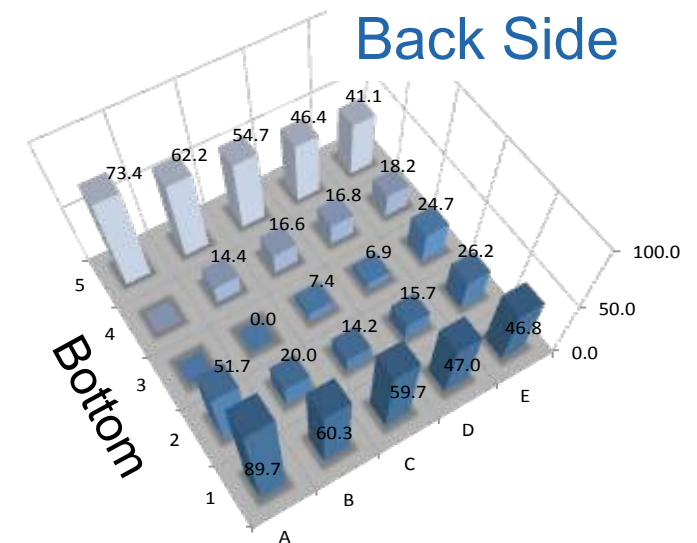
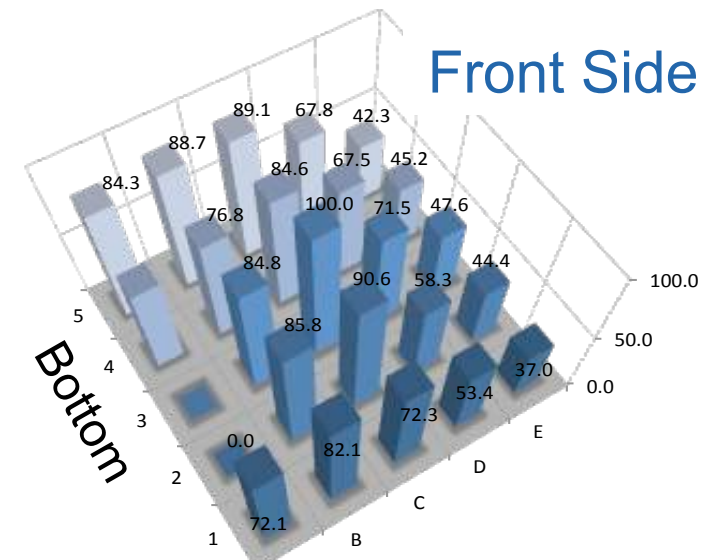
## Experimental Solver Validation: Pyramid Model



# Evaluate Experiments - 2016

## Measuring the Coating Thickness

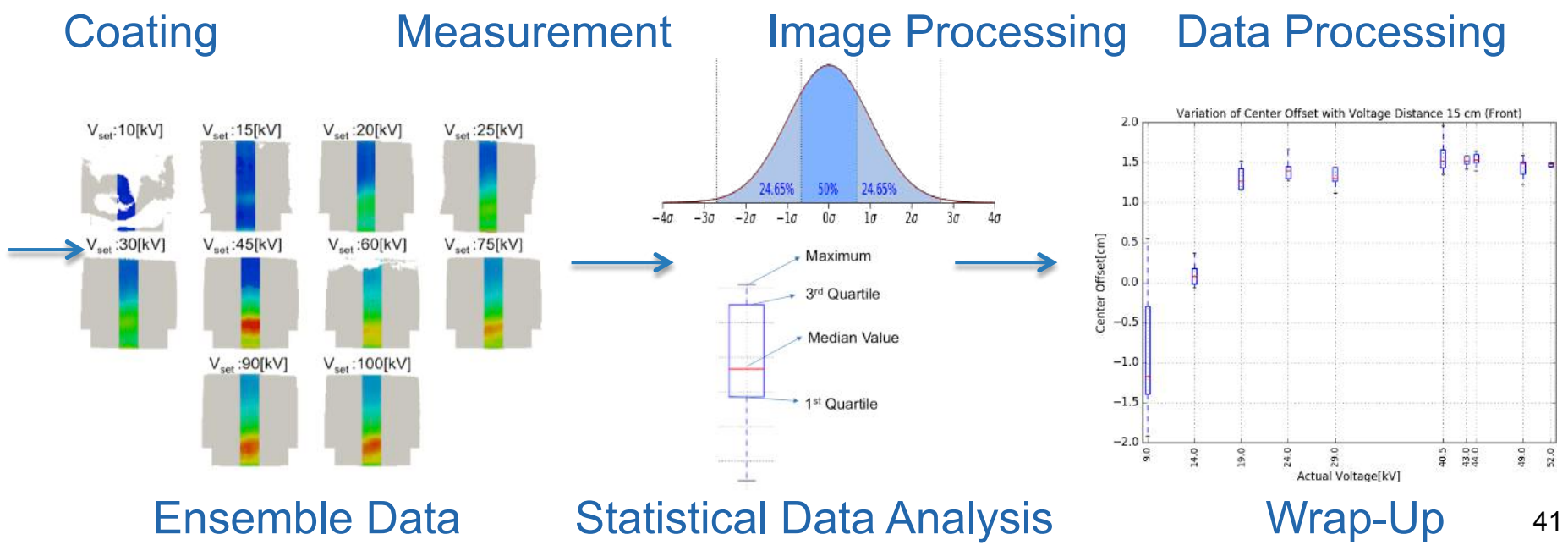
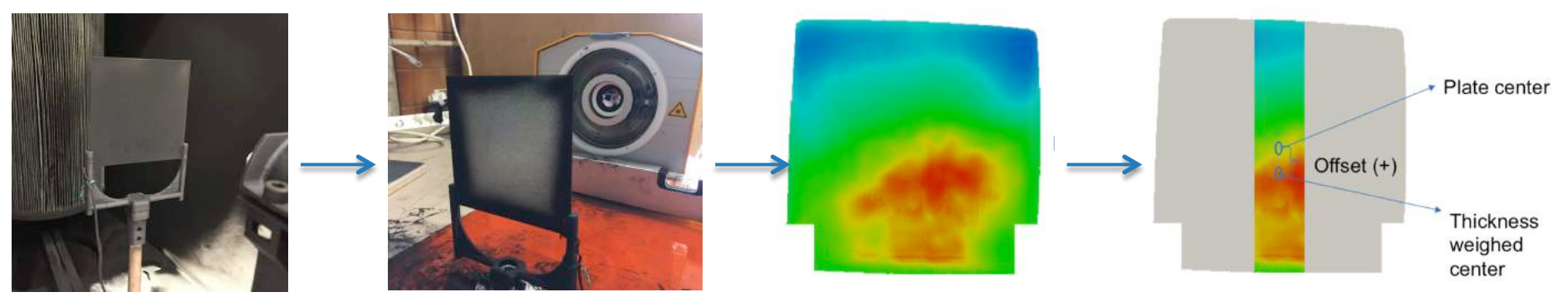
Thermal Measurement of Thickness with Coatmaster





# Evaluate Experiments - 2016

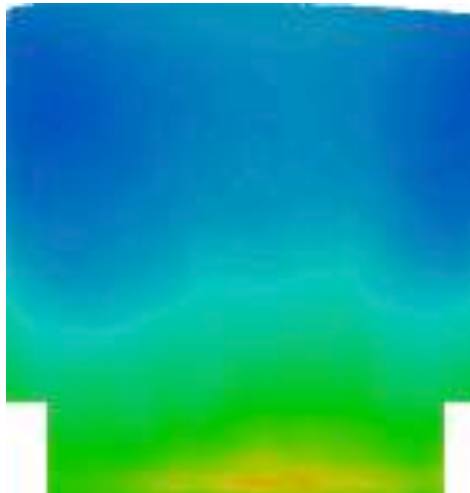
## Development of Instant Evaluation Procedure:



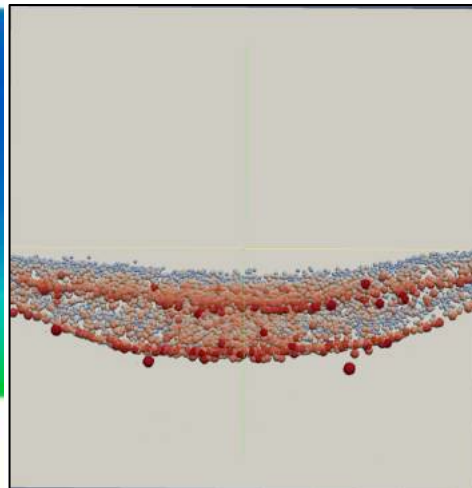
# Comparing - 2016

## Problems with initial Matching: Coating Patterns

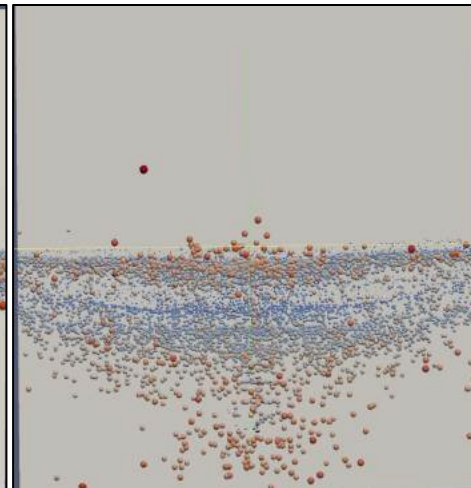
Experiment



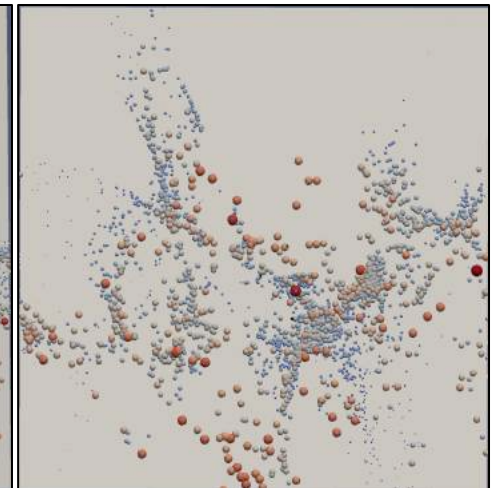
Attempt: A



Attempt: B



Attempt: C



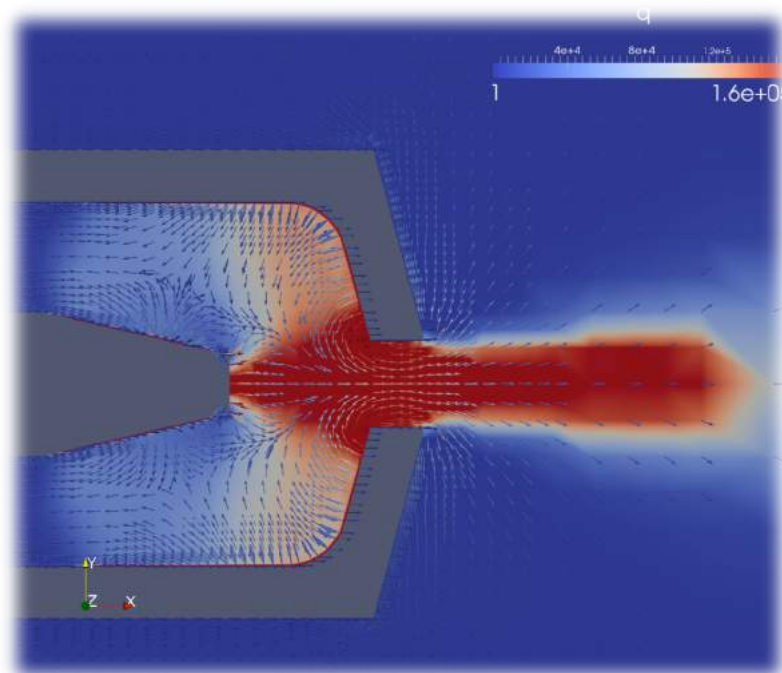
# ICM 2017 - Beijing



Source: <https://www.multiphysics.org/past-conferences>



## Dynamic 3D Modelling of Ionized Oxygen Distribution within Powder Coating Applications

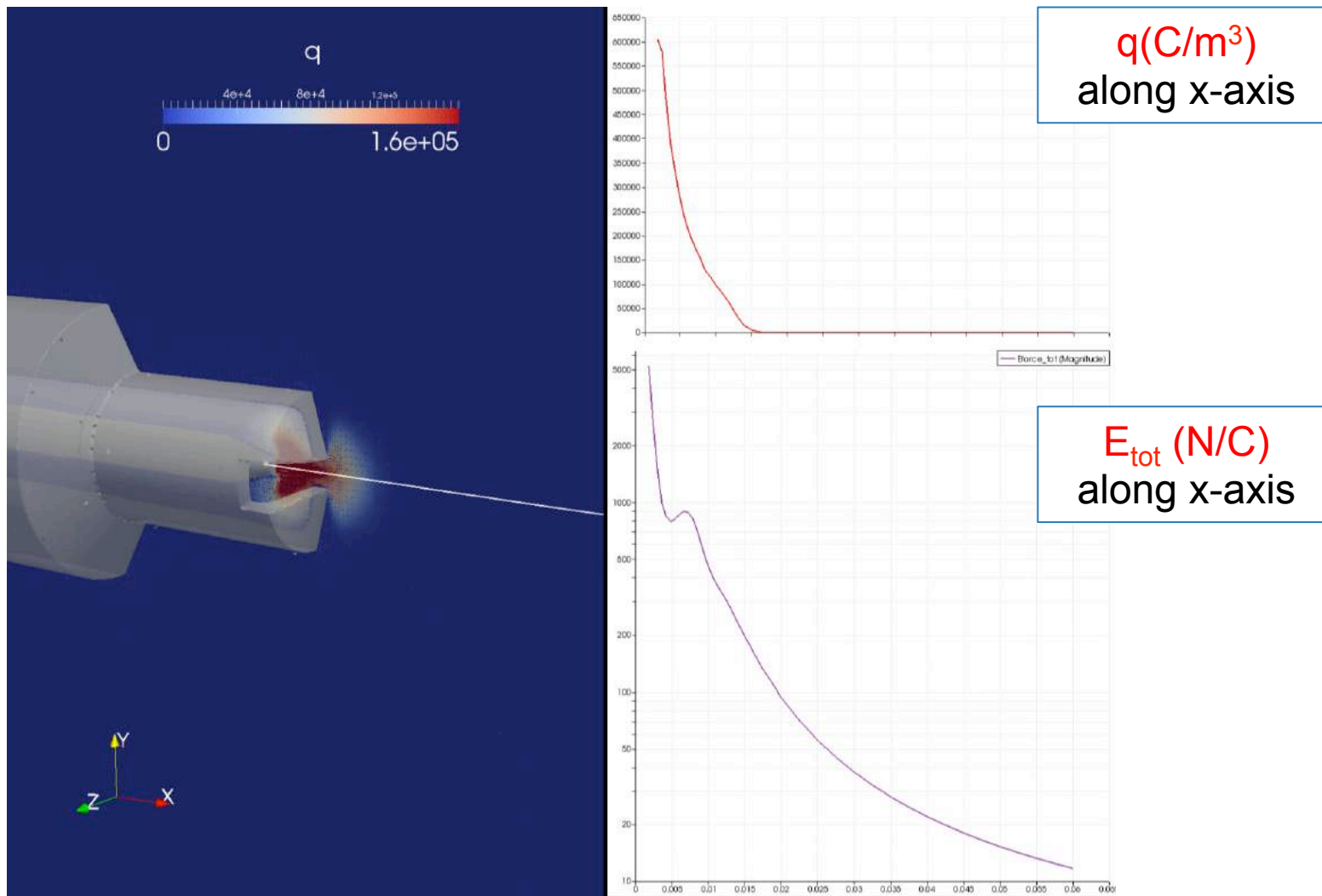


International Conference of Multiphysics, Peijing,  
December 2017, G. Boiger, M. Boldrini, S. Weilenmann

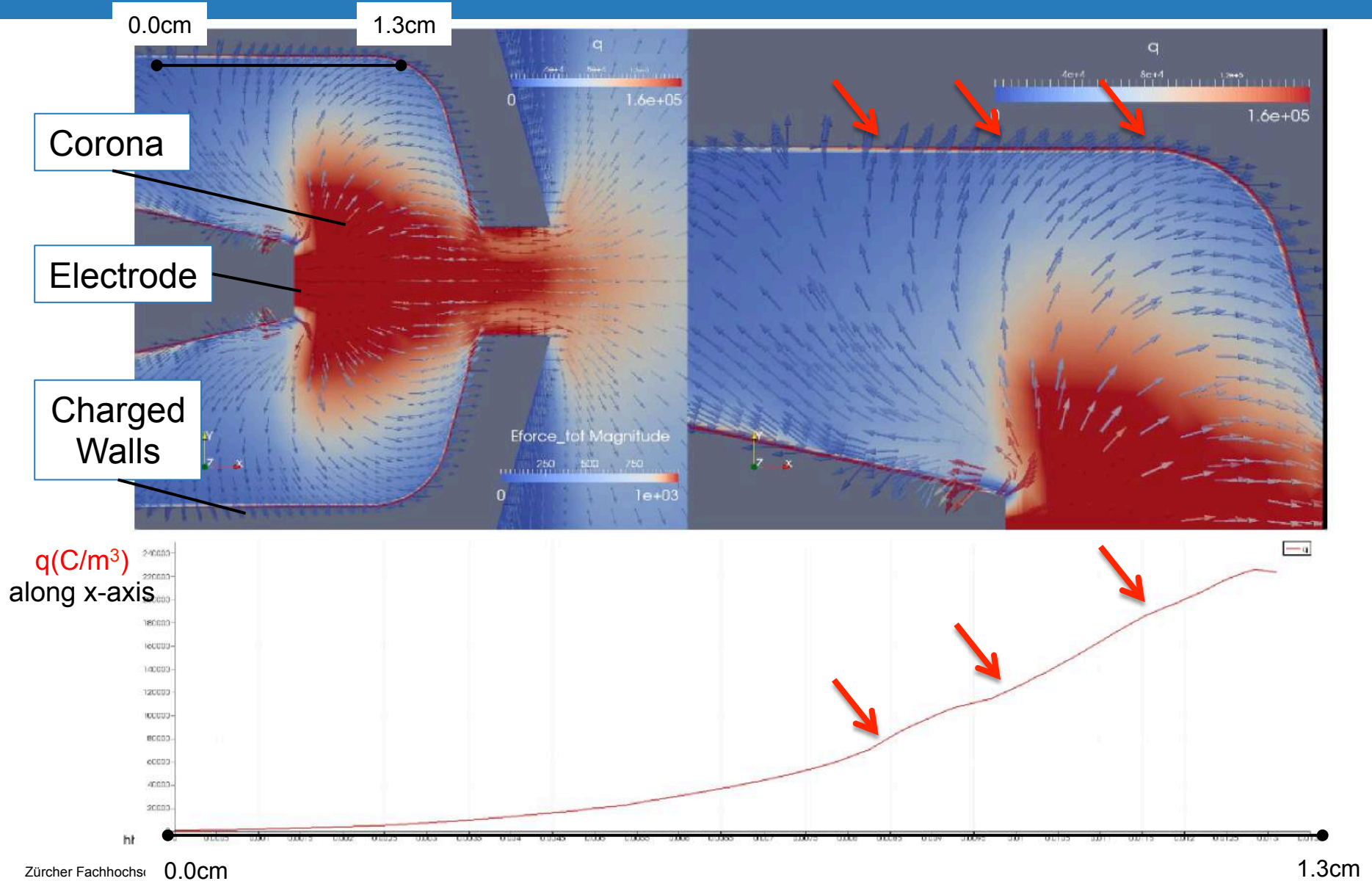


# ICM 2017 - Beijing

## Evolution Step: Space Charge Model

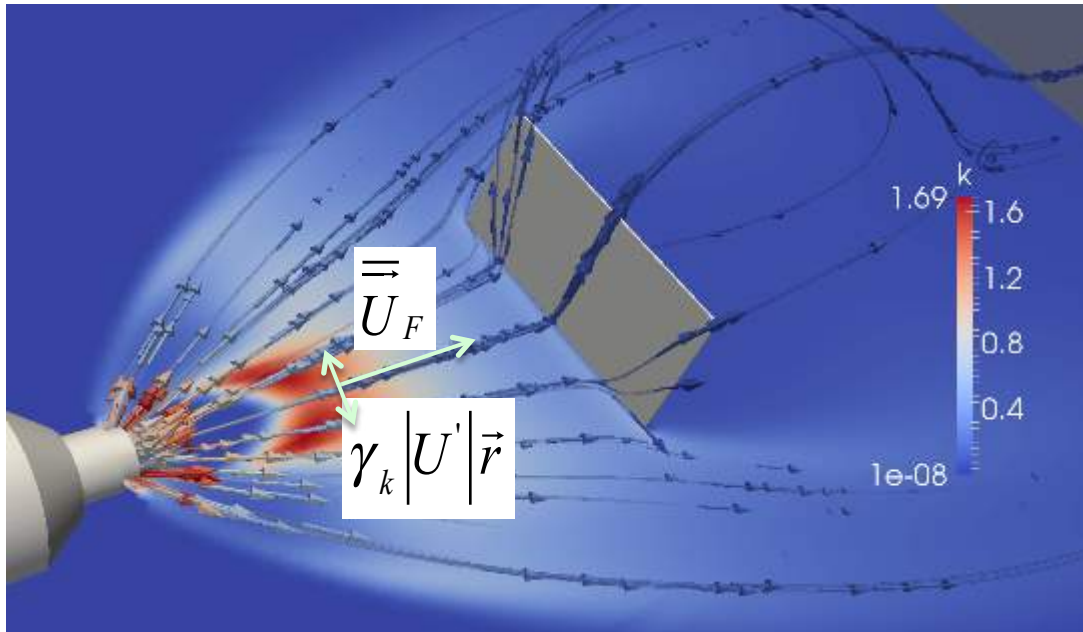


# ICM 2017 - Beijing



# ICM 2017 - Beijing

## Evolution Step: The k-Factor



- $k$  ... Turbulent Kinetic Energy (J/kg)
- $\vec{r}$  ... Randomly oriented Vector Length 1 (-)
- $\overline{\overline{U}}_F$  ... RAS averaged Flow Velocity (m/s)
- $U'$  ... Fluctuating Velocity Component (m/s)

## Assumption of Isotropic Turbulence

$$k = \frac{3}{2} \left[ \overline{(u')^2} + \overline{(v')^2} + \overline{(w')^2} \right]$$

$$k = \frac{3}{2} \overline{(U')^2} \iff |U'| = \sqrt{\frac{2}{3} k}$$

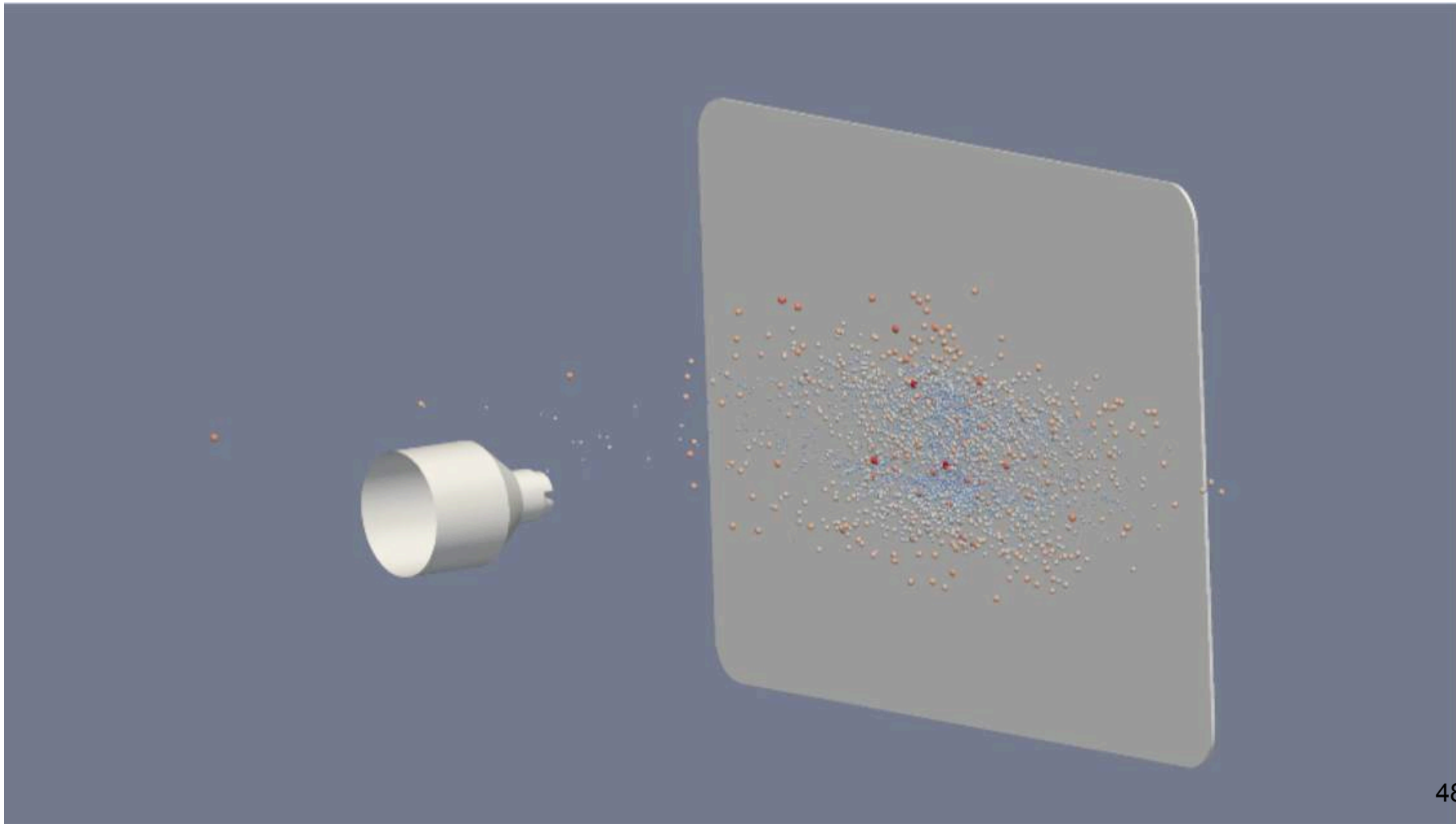
## Modified Flow Velocity acting on Particles

$$\overline{\overline{U}}_{F, \text{mod}} = \overline{\overline{U}}_F + \gamma_k |U'| \vec{r}$$

Empirical  
„k-Factor“

# ICM 2017 - Beijing

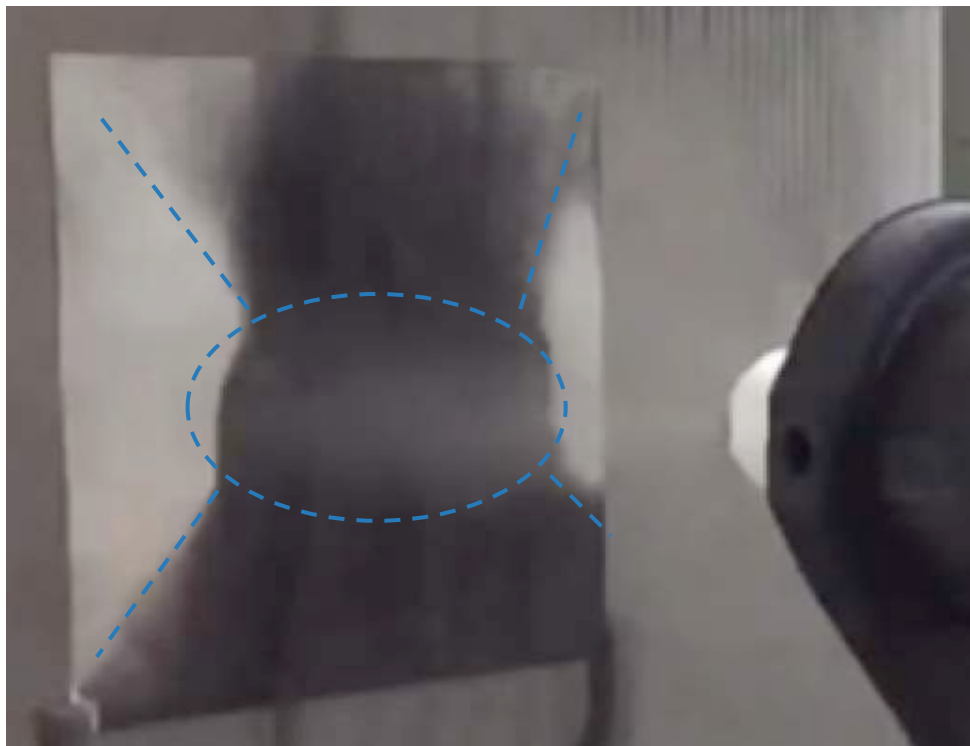
## Evolution Step: Particle - Substrate Interaction



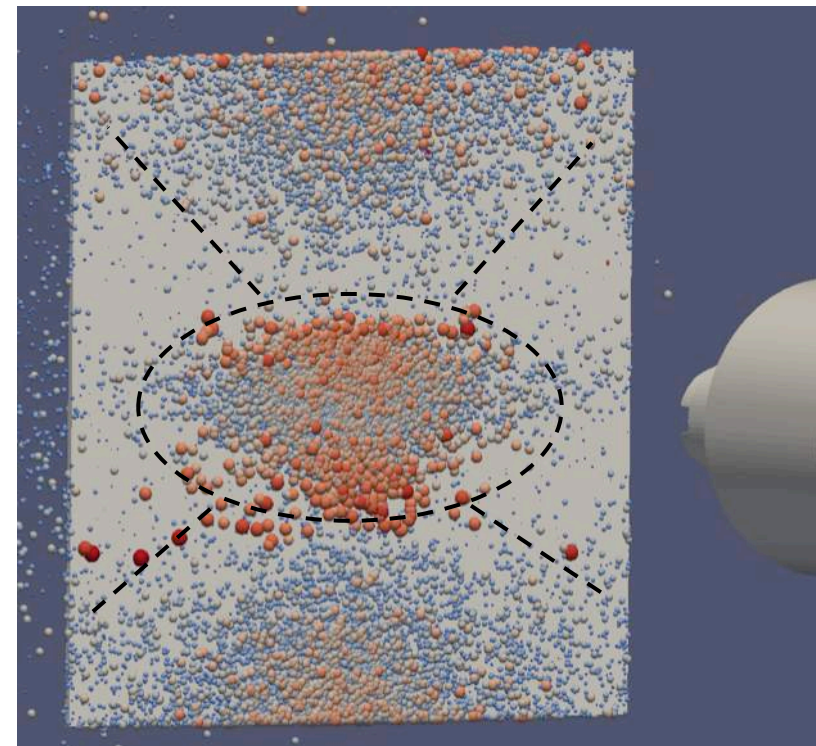


# Next Stage Validation - 2017

## Qualitative Validation: Coating Process in Motion



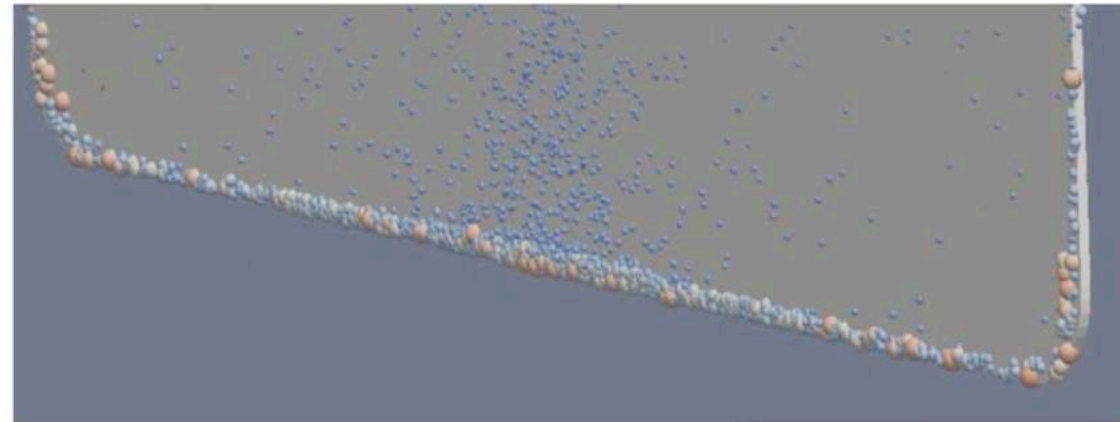
Experiment



Simulation

# Next Stage Validation - 2017

## Qualitative Validation: Dynamic Development of Window Frame



Simulation vs. Experiment





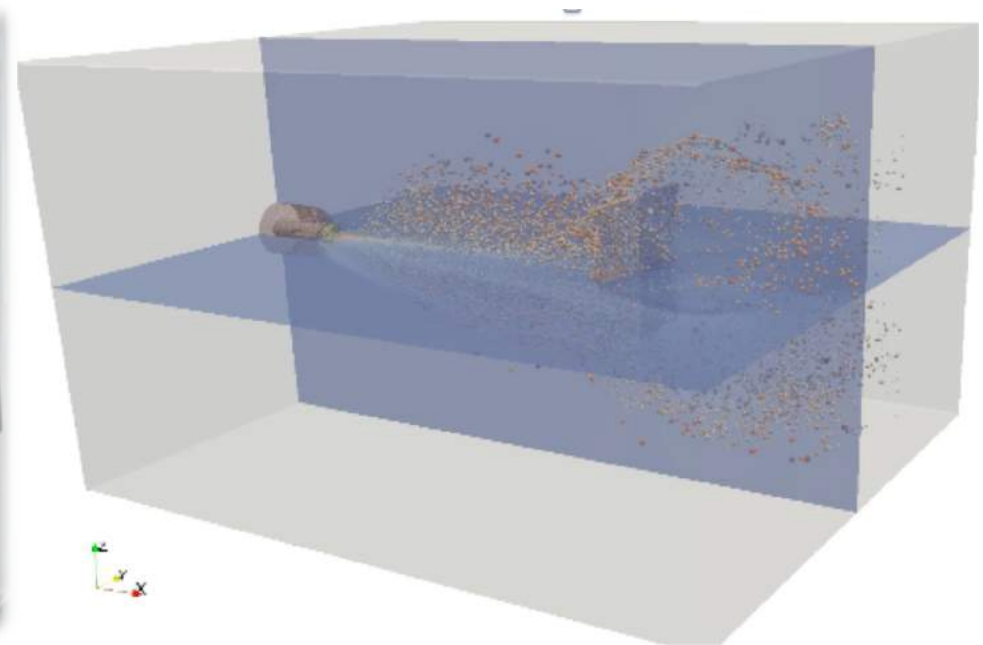
# ICM 2018 - Krakow



Source: <https://www.multiphysics.org/past-conferences>

# ICM 2018 - Krakow

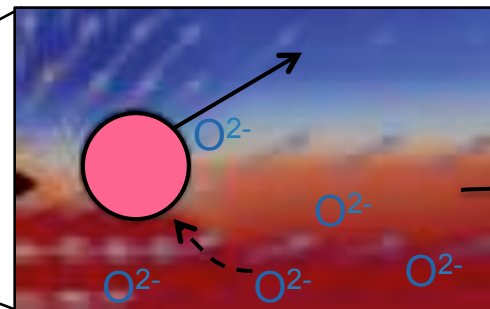
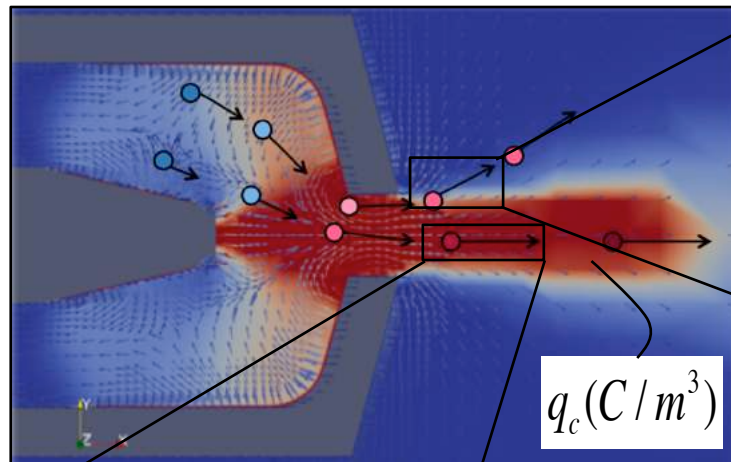
## Enhancing the Understanding of Complex Phenomena in Powder-Coating by Applying Eulerian-LaGrangian Simulation Technology



International Conference of Multiphysics 2018, Krakau, Poland  
13-14<sup>th</sup> Dec 2018, G. Boiger, B. Siyahhan, M. Boldrini, V. Lienhard



## Evolution Step: Dynamic Charging Model



Charging model:

$$\frac{dq_p}{dt} = \beta_{cp} \left( 1 - \frac{q_p(t)}{q_{p,\text{lim}}} \right) \left[ q_c(\vec{X}, t) - \frac{6}{D_p} q_p(t) \right]$$

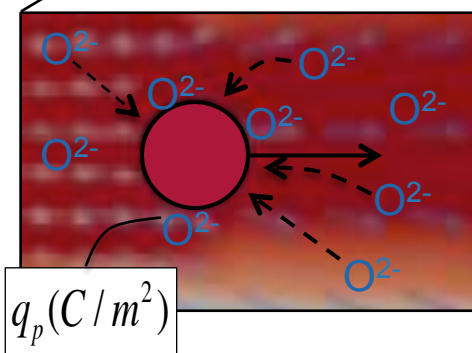
$$q_{p,\text{lim}} = D_p^2 \pi \epsilon_0 |\vec{E}| \cdot \left( 1 + 2 \cdot \frac{\epsilon_{r,p} - 1}{\epsilon_{r,p} + 1} \right)$$

$q_p(\text{C}/\text{m}^2)$  ... Particle Surface Charge

$q_{p,\text{lim}}(\text{C}/\text{m}^2)$  ... Max. Particle Surface Charge

$q_c(\text{C}/\text{m}^3)$  ... Corona  $\text{O}^{2-}$  Charge Density

$\beta_{cp}(\text{m}/\text{s})$  ... Charge Transfer Coefficient

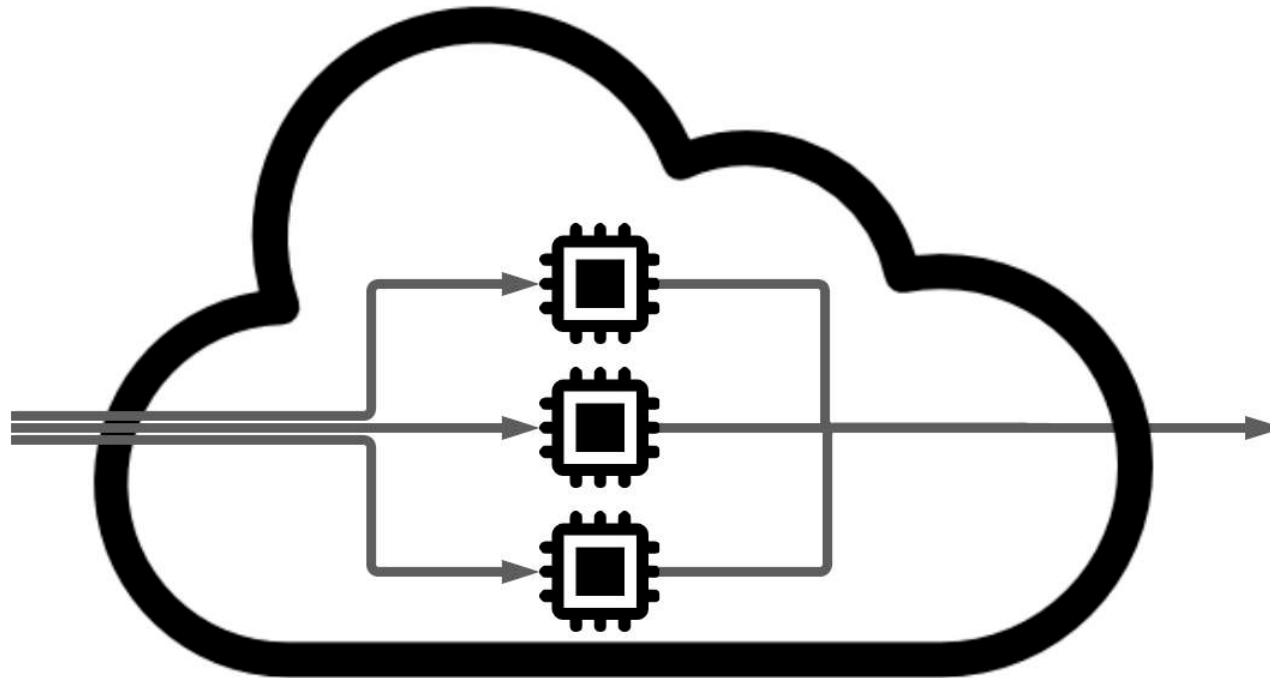


# ICM 2020 - Online



Source: <https://www.multiphysics.org/past-conferences>

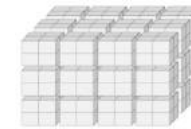
## Introducing Massive Simultaneous Cloud Computing (MSCC) for Multiphysics-Simulation Applications



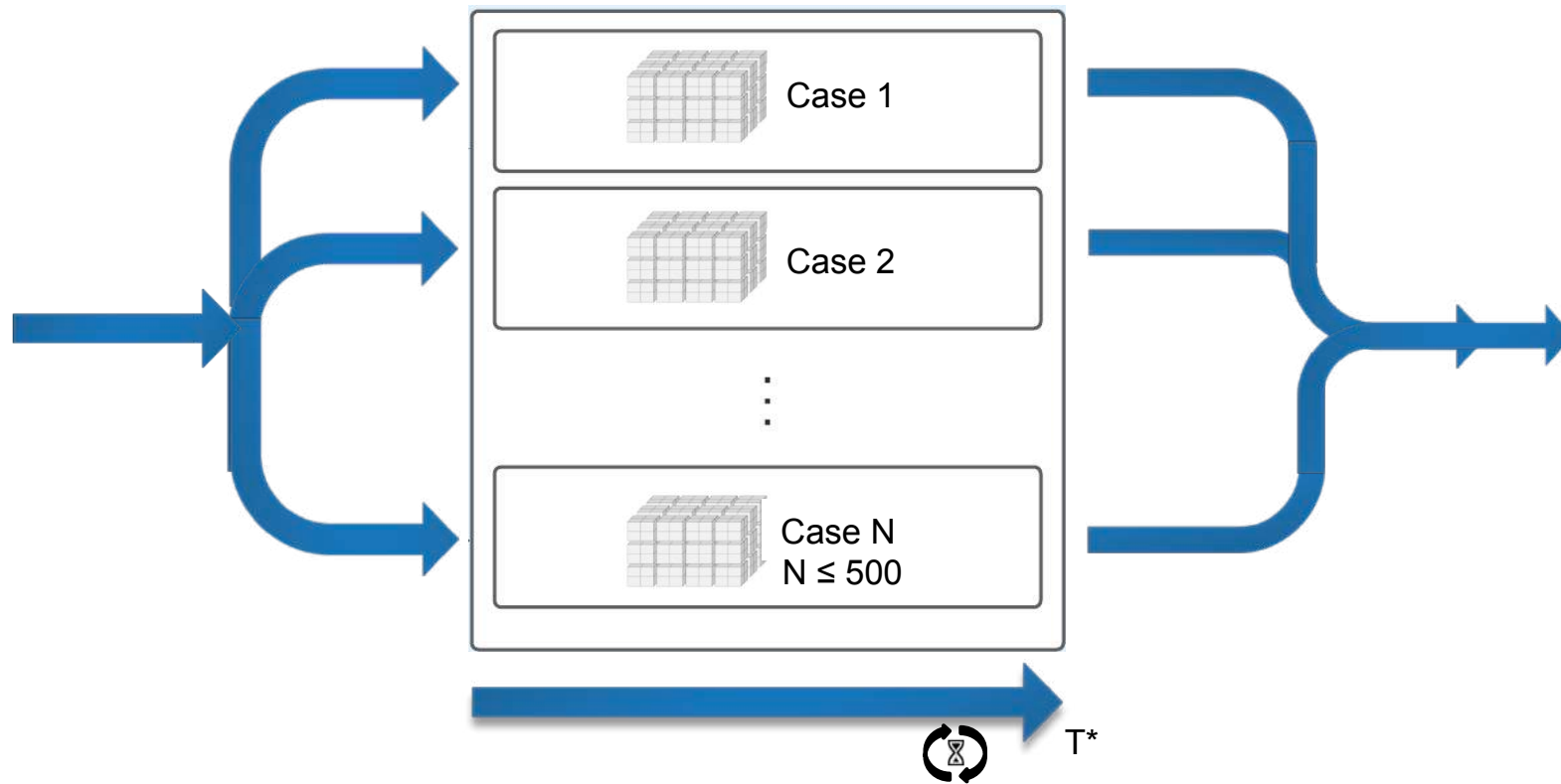
International Conference of Multiphysics 2020, Online

10-11<sup>th</sup> Dec 2020, G. Boiger, D. Sharman, M. Boldrini, M. Everitt

# ICM 2020 - Online



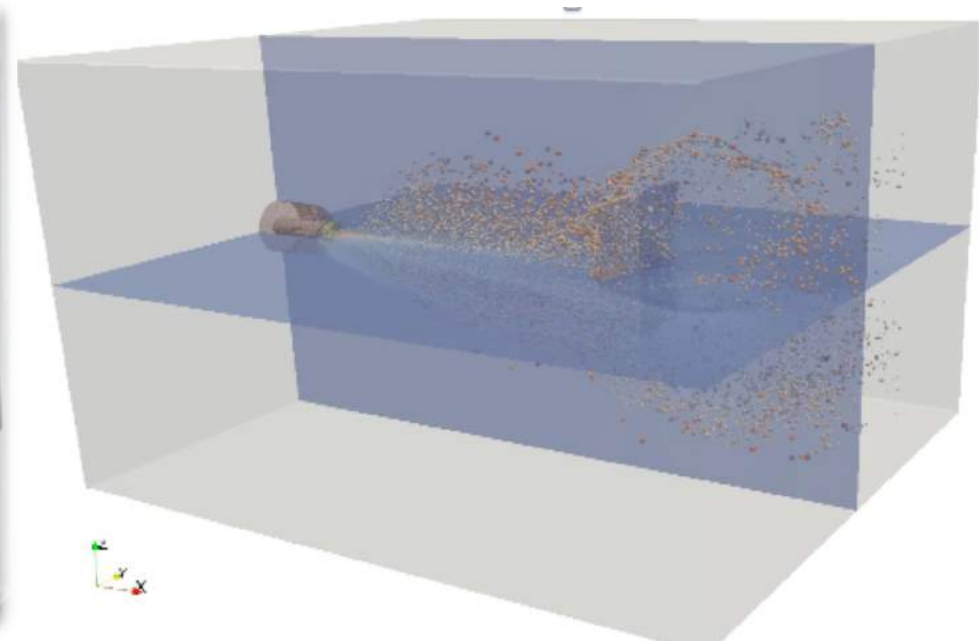
Up to 224 vCPUs per machine



$T^*$  .... Wall Clock Time to calculate one Single Case



## Advancing the Validation and Application of a Eulerian-Lagrangian Multiphysics Solver for Coating Processes in Terms of Massive Simultaneous Cloud Computing

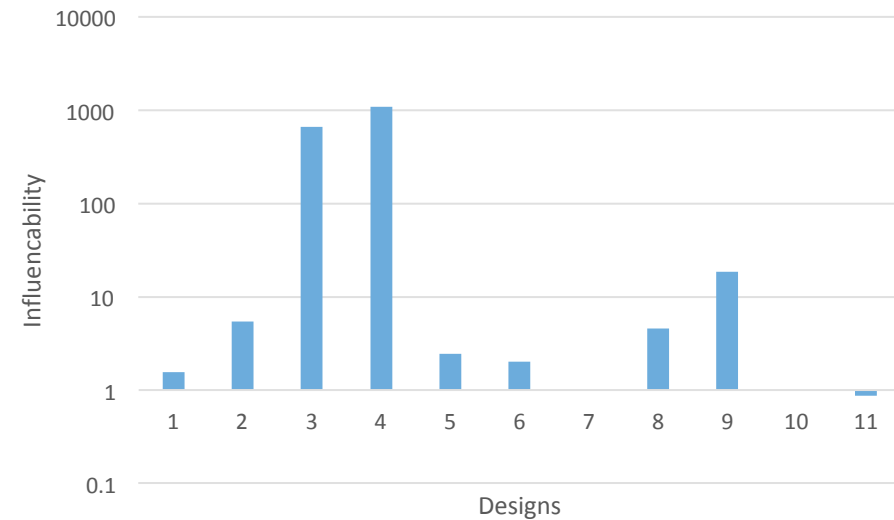
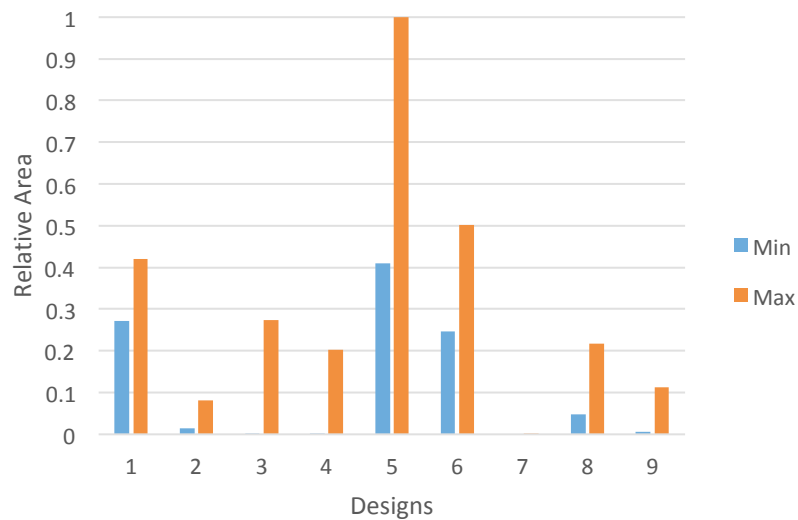
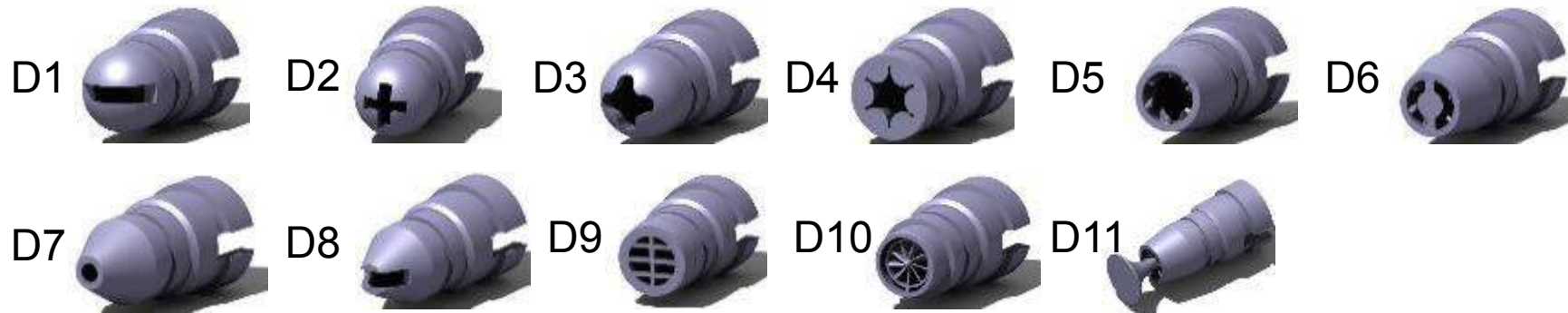


International Conference of Multiphysics 2020, Online

10-11<sup>th</sup> Dec 2020, G. Boiger, B. Siyahhan, M. Boldrini, V. Lienhard

# ICM 2020 - Online

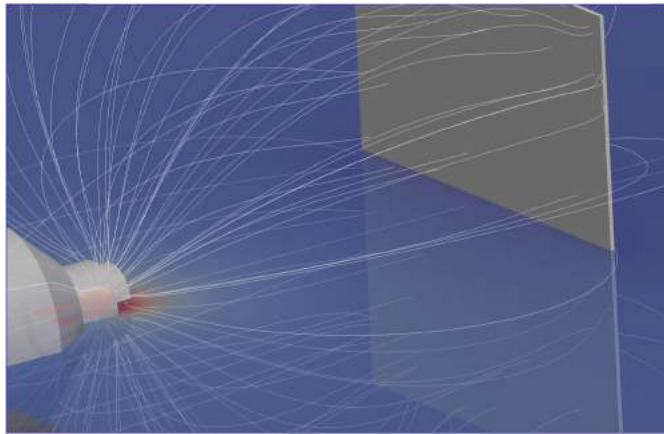
## Cloud Simulation based Prototyping



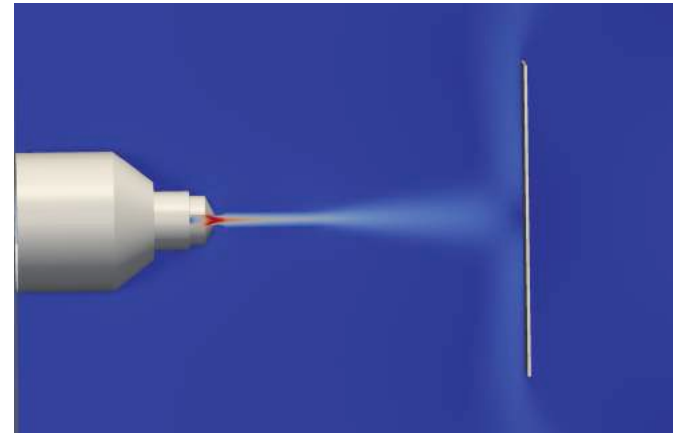
17<sup>th</sup> Int. Conference of Multiphysics 2022, Oslo  
G.Boiger; Keynote; 15.12.22

# ICM 2020 - Online

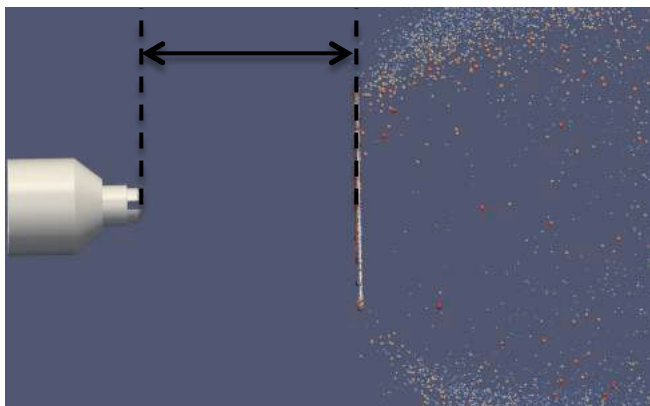
## Experimental Solver Validation: Vary Process Parameters



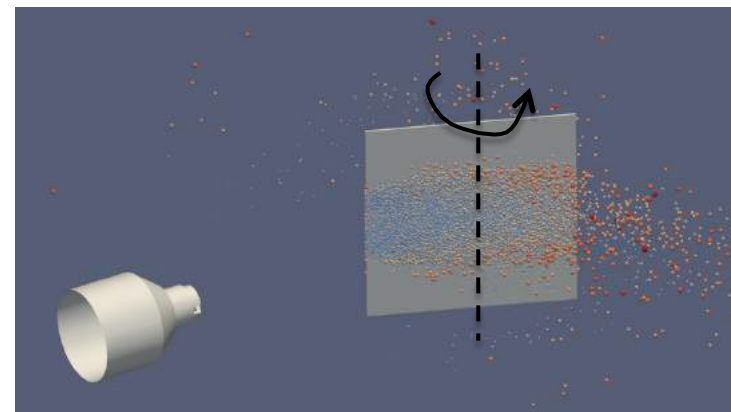
Voltage: 0kV-100kV



Flow-Rate: 2m<sup>3</sup>/min – 5m<sup>3</sup>/min

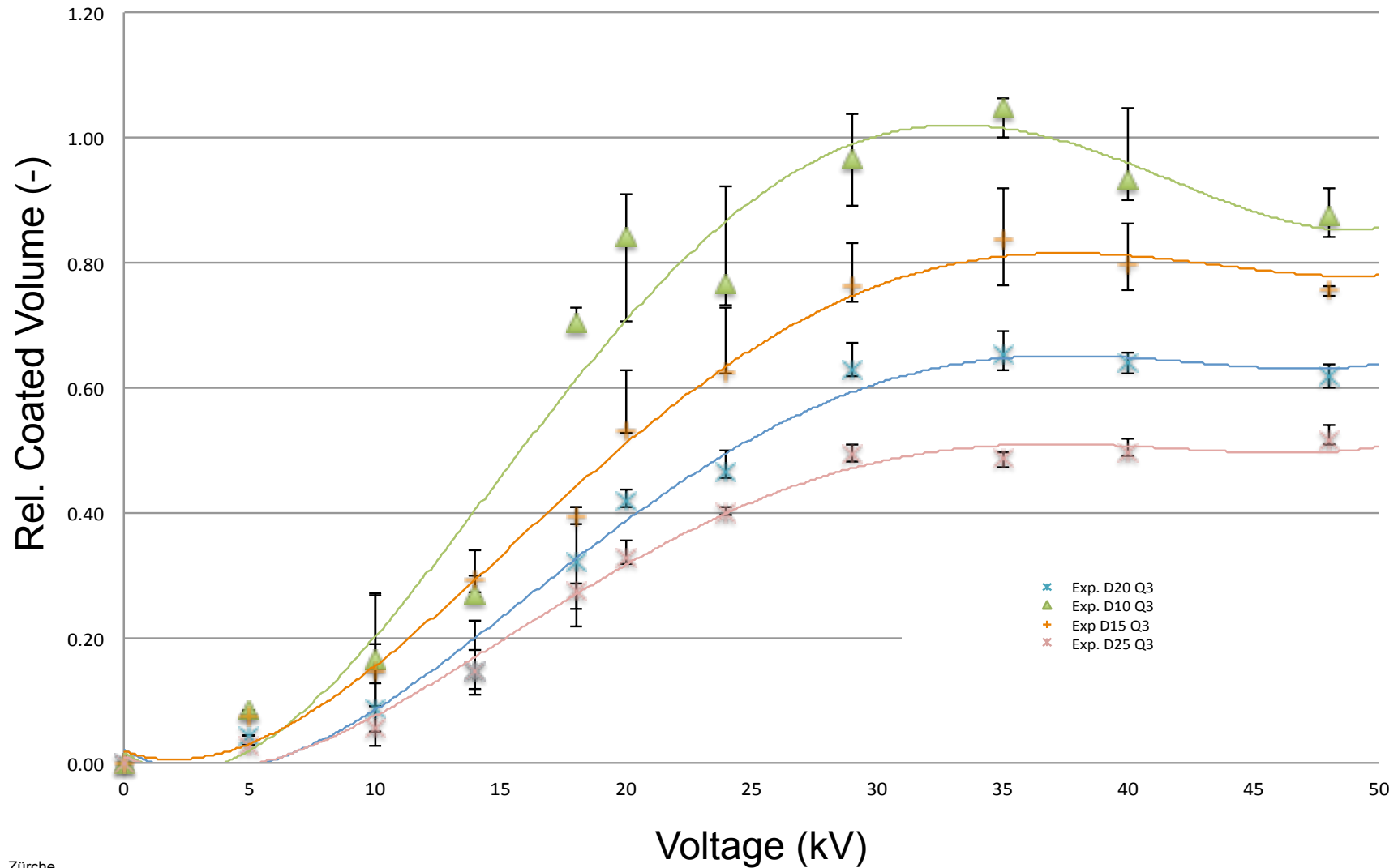


Distance: 10cm – 25cm



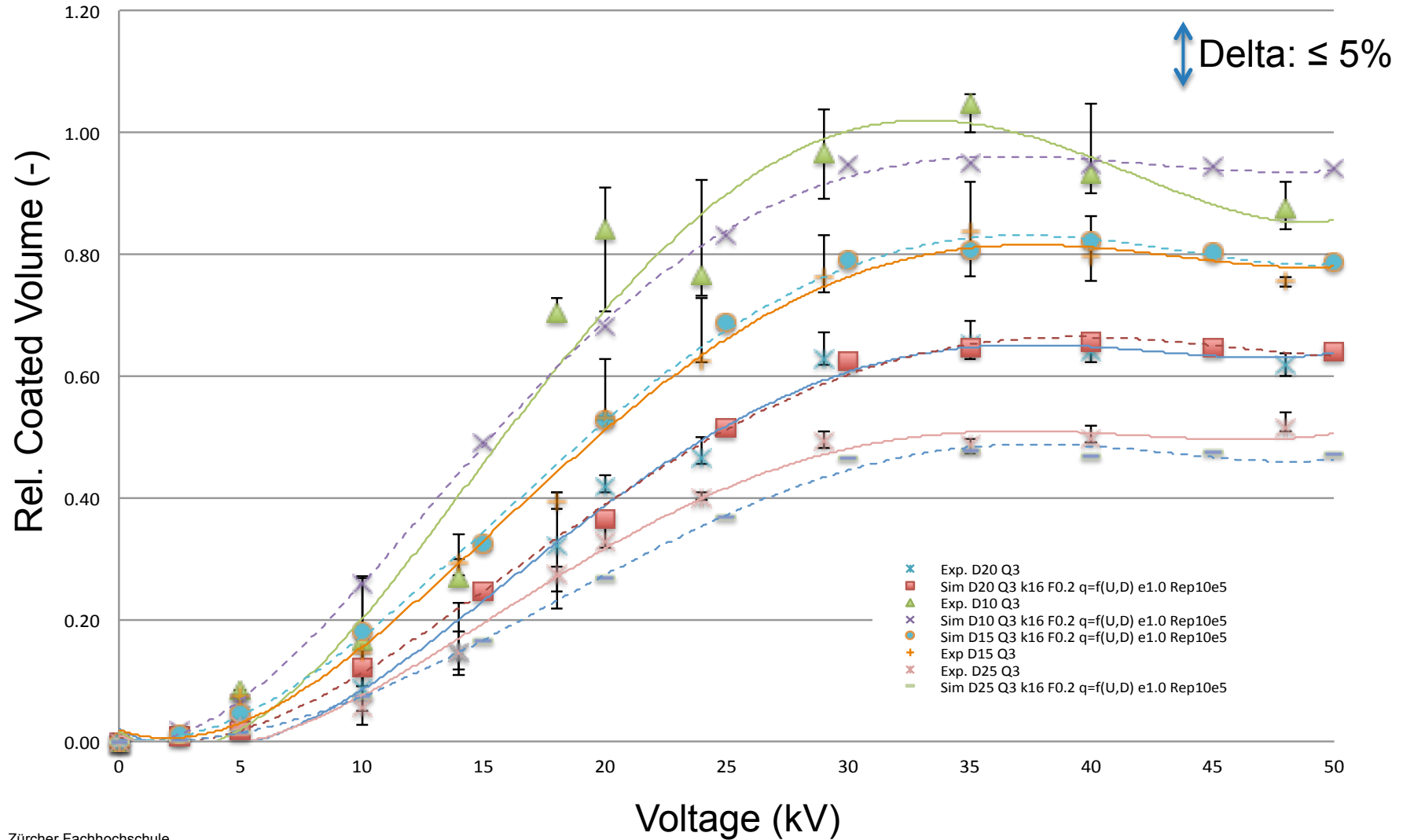
Angle: 0° - 90°

## Quantitative Validation





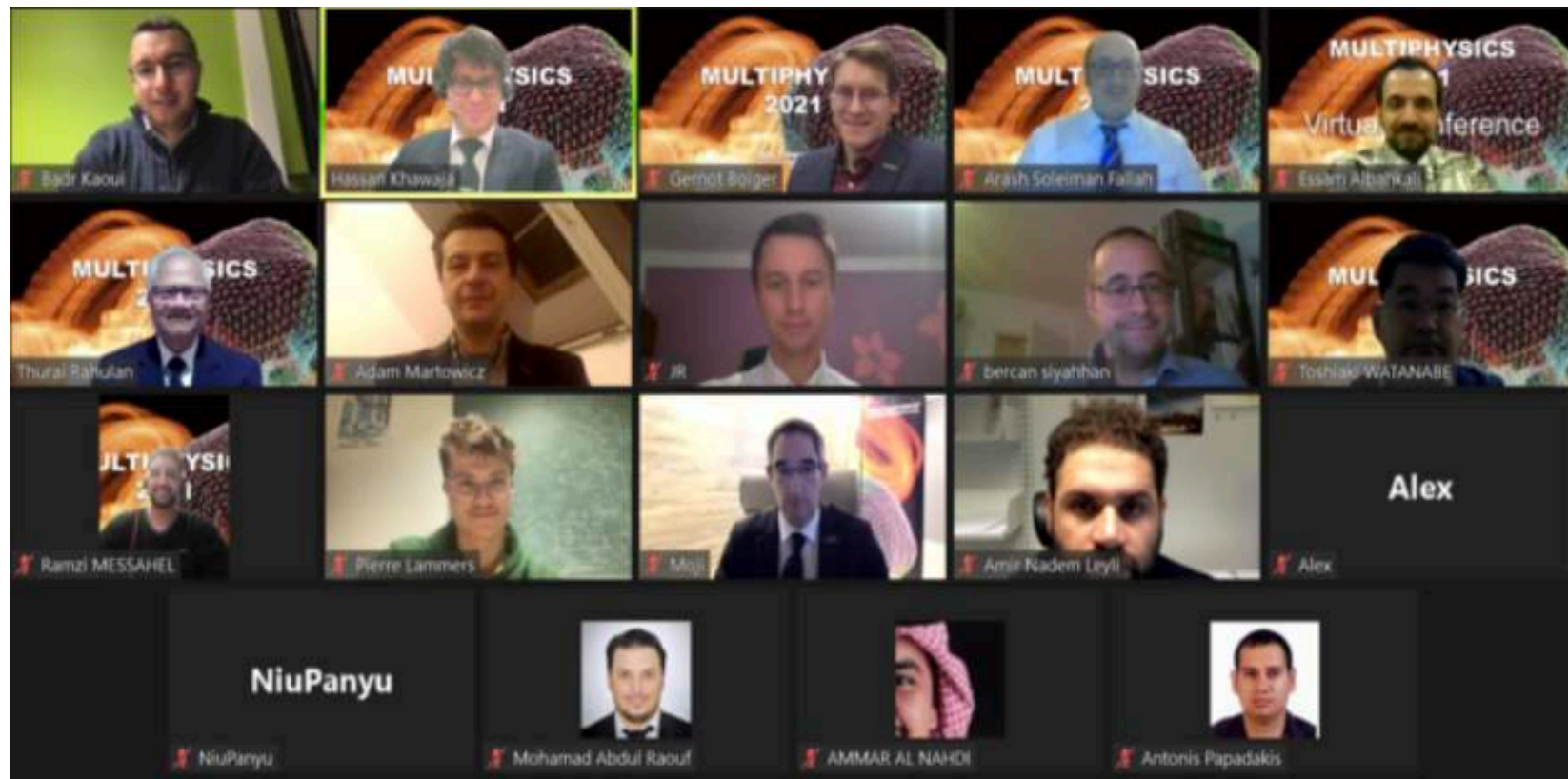
## Quantitative Validation



# ICM 2021 - Online

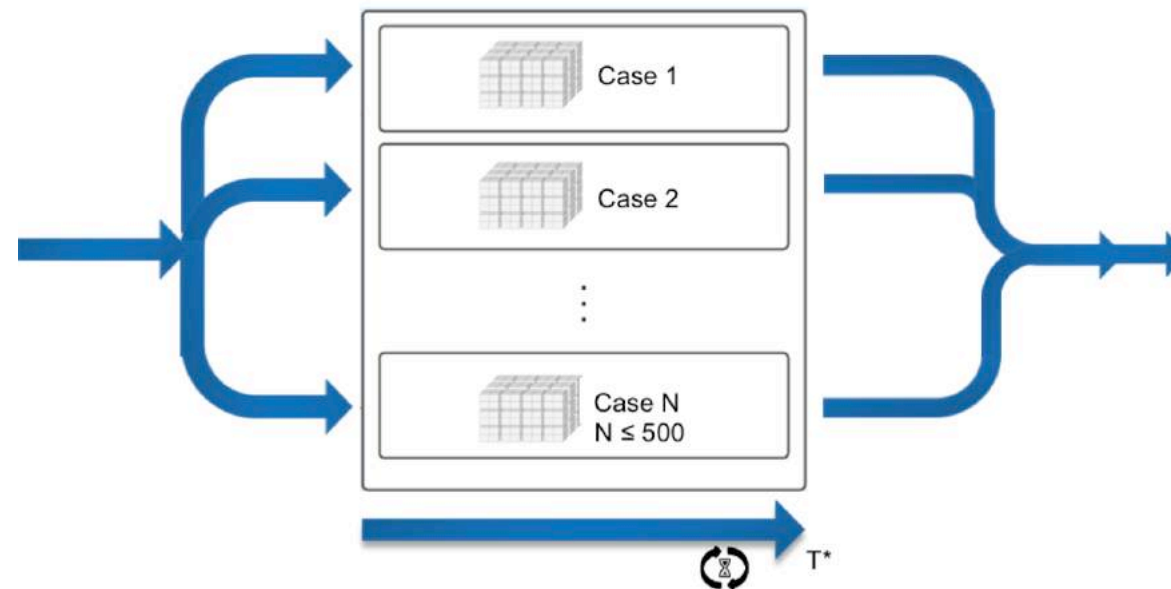
Zürcher Hochschule  
für Angewandte Wissenschaften

**zhaw** School of Engineering  
ICP Institute of Computational Physics



Source: <https://www.multiphysics.org/past-conferences>

## A Massive Simultaneous Cloud Computing Platform for Multiphysics Simulations



16<sup>th</sup> International Conference of Multiphysics 2021, Online  
9<sup>th</sup>-10<sup>th</sup> Dec 2021, G. Boiger, D. Sharman, D. Drew, D. vanOerle, S. Delbari

# Workflow: Motorbike

- Case: Motorbike
- Size of mesh: 300k cells
- Solver: simpleFoam
- Parameter Study: 160 cases
- MSCC on KaleidoSim: AMD Epyc Rome; 2.25-2.7GHz
- Each case parallelized on: 4 vCPU





### 3. Towards Industrial Application



# Content

## A Semi-Automated Multiphysics Simulation Software for Process Design in the Powder Coating Industry



Bercan Siyahhan ([siya@zhaw.ch](mailto:siya@zhaw.ch))

Prof. Dr. Gernot Boiger ([boig@zhaw.ch](mailto:boig@zhaw.ch))

# ICM 2021 - Online



# ICM 2021 - Online

coatSim

- Set Working Directory
- Geometry
- Motion / Align Interface
- Mesh
- Solver Definition
- Material & Process Properties
- Simulation
- Quit

Motion Definition

Pistol: pistol\_0

Motion Type: Translational

Motion Function: Fourier Series

Motion Start Time [s]: 0.2

Motion End Time [s]: 0.5

Motion Period [s]: 0.1

Sine Coeffs. separated by "," bn n=1,..: 0.23,-0.039,-0.022

Cosine Coeffs. separated by "," an n=0,..: 0.43,-0.33,-0.10,0.05,-0.02

Translation Direction X component:

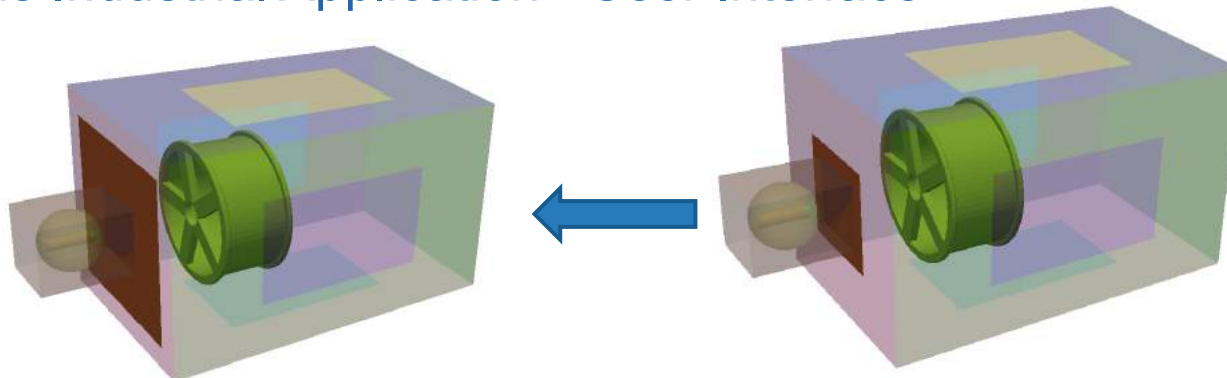
Translation Direction Y component: 0.1

Translation Direction Z component: 0.1

Buttons: Set, Apply Motion, Finish/Align, Delete & Quit, Quit

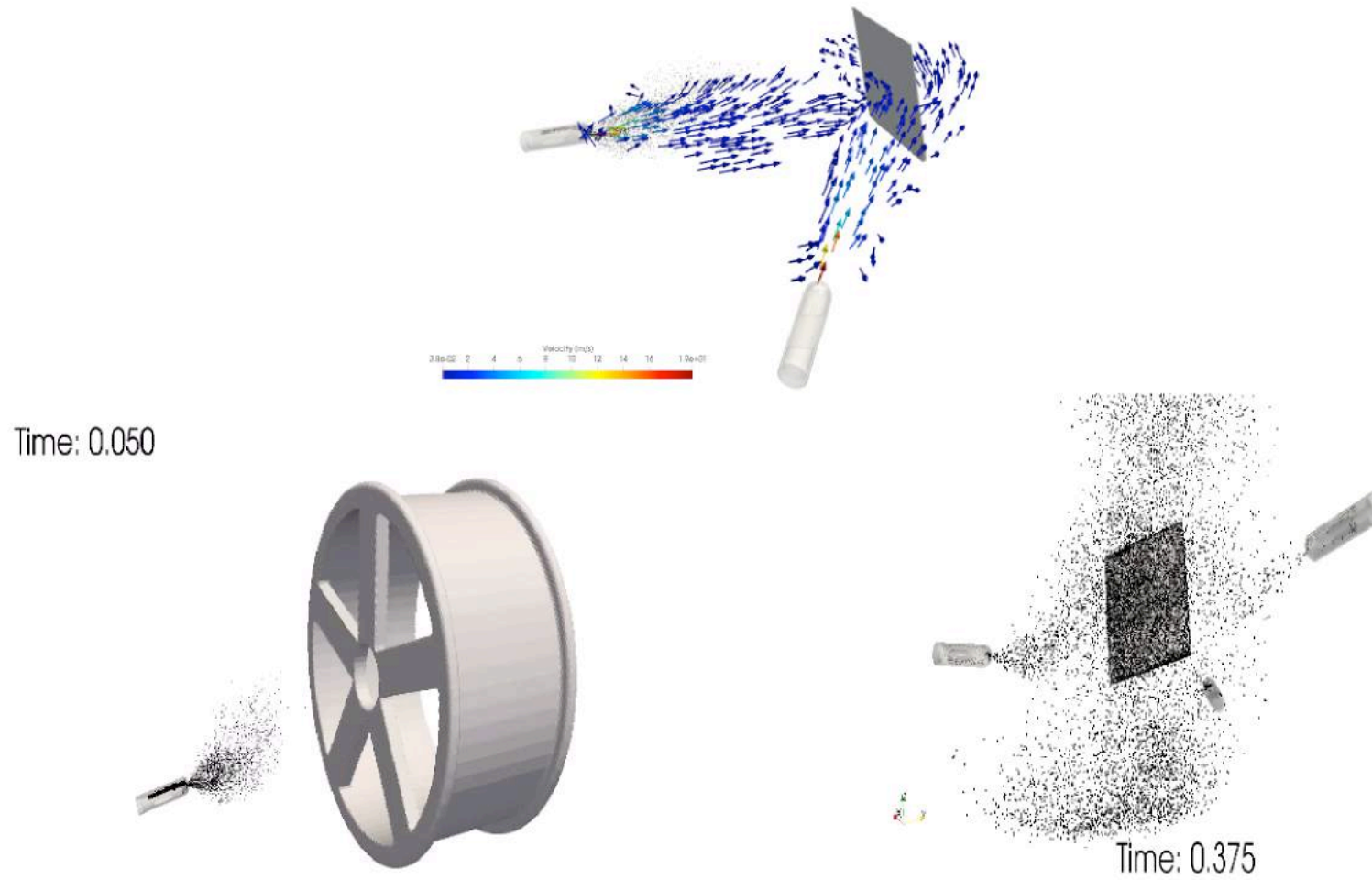
$$f(t) = \sum_{n=0}^{\infty} a_n \cos \frac{2\pi n t}{T} + \sum_{n=1}^{\infty} b_n \sin \frac{2\pi n t}{T}$$

## Towards Industrial Application - User Interface





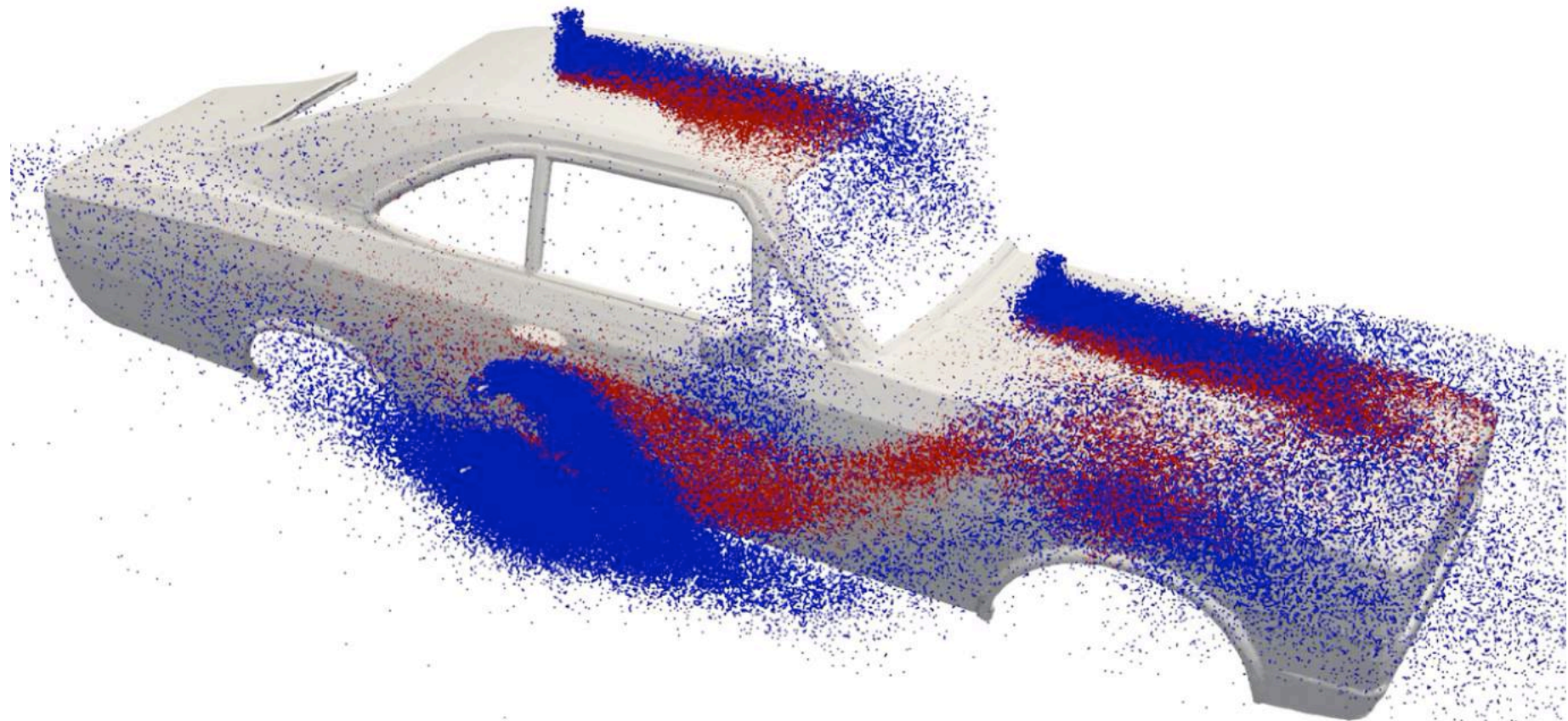
# ICM 2021 - Online



# CoatSim in Action - 2022

Time: 4.500

BoundaryStatus  
0.0e+00 1.0e+00

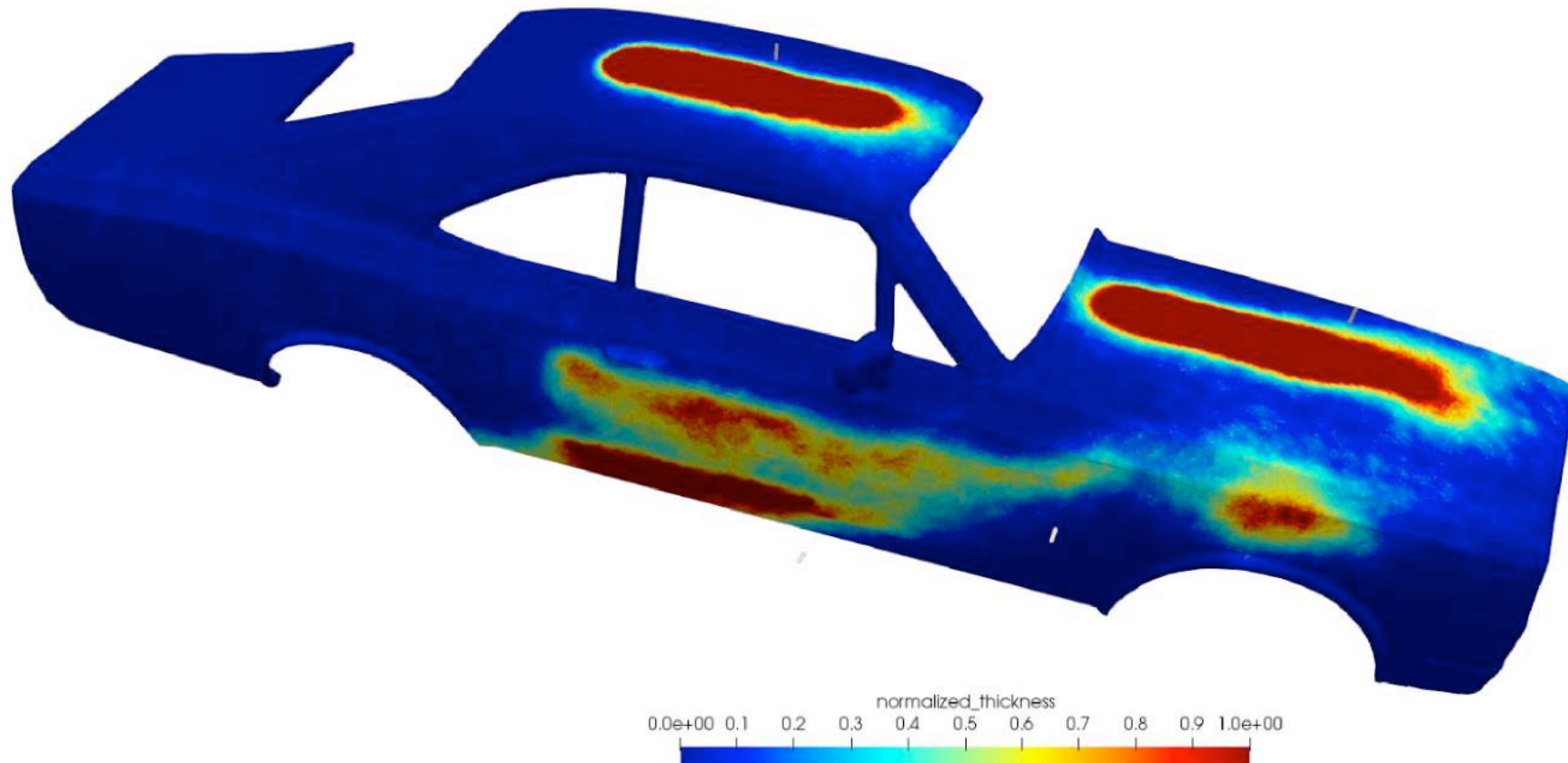


# CoatSim in Action - 2022

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für Angewandte Wissenschaften

**zhaw** School of Engineering  
ICP Institute of Computational Physics

Time: 8.000



## 4. Outlook



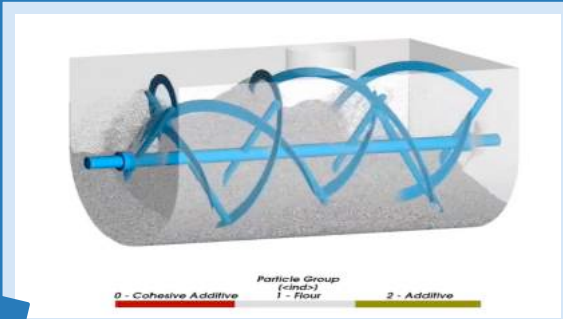
# Content



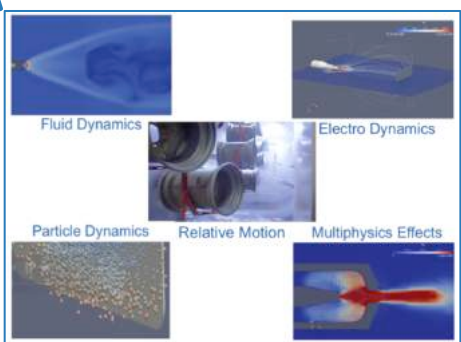
# Outlook



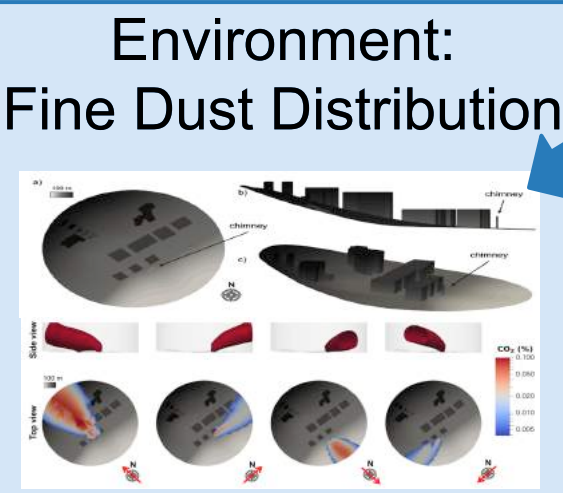
**Production:  
Galvanization**



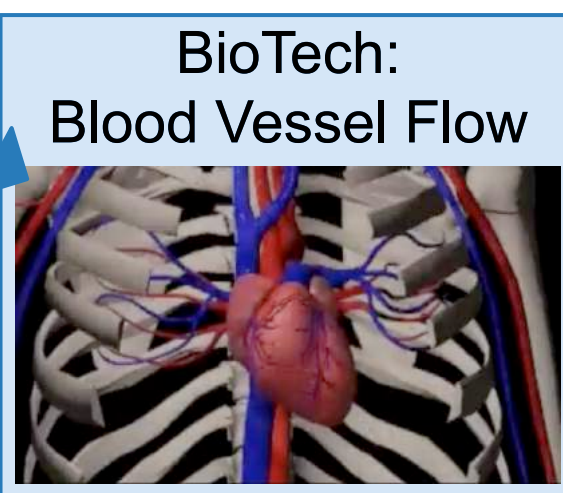
**Pharma:  
Mixing**



**Environment:  
Fine Dust Distribution**



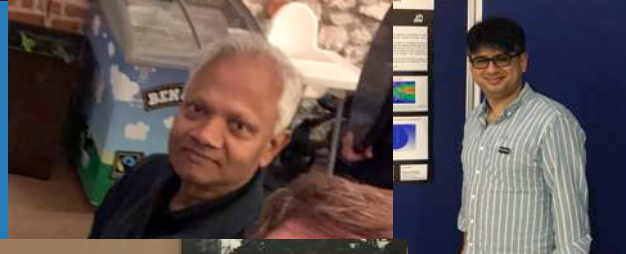
**BioTech:  
Blood Vessel Flow**



**Modular  
Physical Model**



So what is it all for?



Thank you for your attention!

Content